FOUR CORNERS POWER PLANT Lined Ash Impoundment, Lined Decant Water Pond, Combined Waste Treatment Pond, Upper Retention Sump, and Dry Fly Ash Disposal Area

# Annual CCR Impoundment and Landfill Inspection Report

2018



GENERATION ENGINEERING Design Engineering P.O. BOX 53999 PHOENIX, ARIZONA 85072

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#### **1.0 INTRODUCTION**

Arizona Public Service Company (APS) prepared this report to comply with the Environmental Protection Agency's (EPA) <u>Hazardous and Solid Waste Management System; Disposal of Coal</u> <u>Combustion Residuals From Electric Utilities; Final Rule</u> (2015) requiring "...inspections by a qualified professional engineer at intervals not exceeding one year to ensure that the design, construction, operation, and maintenance of the CCR unit is consistent with recognized and generally accepted good engineering standards" (40 CFR 257.83(b)(1) for CCR surface impoundments and 40 CFR 257.84(b)(1) for CCR landfills). AECOM staff participated in the CCR unit inspection and provided technical support in the preparation of this document.

This report includes a review of relevant data in the operating record as well as visual inspections of the Lined Ash Impoundment, the Lined Decant Water Pond, the Combined Waste Treatment Pond, the Upper Retention Sump, and the Dry Fly Ash Disposal Area. The Lined Ash Impoundment and Lined Decant Water Pond are instrumented with piezometers, inclinometers, settlement monuments, and settlement rods.

Inspection Conducted by

Byron R. Conrad, P.E. Consulting Geological Engineer Design Engineering Generation Engineering Arizona Public Service Company



Lee M. Wright, P.E. Geotechnical Engineer AECOM 7720 North 16<sup>th</sup> Street, Suite 100 Phoenix, Arizona

2018 Annual CCR Impoundment and Landfill Inspection Report APS Four Corners Power Plant

January 2019

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# 2.0 SITE BACKGROUND AND INSPECTION CONDITIONS

The Four Corners Power Plant (FCPP, the Plant) is located in Fruitland, New Mexico, approximately 20 miles west of Farmington, New Mexico and 13 miles southeast of Shiprock, New Mexico. The Plant is immediately south of Morgan Lake and primarily in Section 36, Township 29 North, Range 16 West on the Navajo Indian Reservation in San Juan County. Units 1, 2, and 3 ceased generation in 2013 and were then decommissioned. Units 4 and 5 burn low sulfur coal and have a total net generating capacity of 1,540 megawatts.

The coal combustion process produces Coal Combustion Residuals (CCR) including; bottom ash (silty sand, Unified Soil Classification System SM), fly ash (low plasticity silt, Unified Soil Classification System ML), and flue gas desulfurization sludge (FGD). The Plant is operated as a low volume water usage system. The Lined Ash Impoundment (LAI) is used for CCR disposal and the Lined Decant Water Pond (LDWP) is used to temporarily store water drained from the LAI. The Dry Fly Ash Disposal Area (DFADA) is a CCR landfill used to dispose of dry CCR from Units 4 and 5. The Upper Retention Sump collects water from drains located on the Plant site and receives CCR in storm water, process water, and Plant washdown from several sources within the Plant. The Combined Waste Treatment Pond (CWTP) is a settling pond for bottom ash sluice water and various storm water, process water, and Plant washdown streams. The CWTP discharges through a NPDES-permitted outfall to Morgan Lake. These five coal combustion waste Units are the subject of this inspection report.

The field inspection was conducted on Wednesday, October 24, 2018 and Thursday, October 25, 2018. Conditions were mild (44-65 degrees Fahrenheit) with cloudy skies on Wednesday morning and partly cloudy to mostly sunny skies Wednesday afternoon and Thursday. Winds were moderate on Wednesday afternoon and lighter on Thursday. Approximately 3.56 inches of precipitation had fallen since the start of the year based on data recorded at the Four Corners Regional Airport in Farmington, New Mexico (NOAA 2018).

Instrumentation at the LAI and LDWP generally consists of open standpipe PVC piezometers, vibrating wire piezometers, inclinometers, settlement monuments, and settlement rods measured using a Global Positioning Survey (GPS) System. Water levels in the open standpipe piezometers are measured with an electronic water level indicator attached to a cable stamped with increments of 0.01 feet. Water level data for the vibrating wire piezometers are downloaded at a central readout box and processed by Plant personnel. Data for the inclinometers, settlement monuments, and settlement rods are also gathered and processed by Plant personnel.

The benchmarks for the elevations reported for GPS surveys of the settlement monuments at the Four Corners Power Plant are based on one of three survey monuments: EMMA, an aluminum cap, and two Southern California Edison (SCE) brass caps – HV-53, and HV-61. The latitude and longitude of the monuments are based on the NAD83 datum. The elevations of EMMA, HV-53, and HV-61 are 5382.251, 5331.214, and 5085.898 feet, respectively.

# **3.0 UNIT DESCRIPTIONS**

# 3.1 LINED ASH IMPOUNDMENT (LAI)

The LAI is represented on Figure 1 – Lined Ash Impoundment (LAI).

The LAI (listed by the New Mexico Office of the State Engineer (NMOSE) Dam Safety Bureau as dam number D-634) was constructed between 2003 and 2014, has a reservoir storage capacity of 5,346 acre-feet, and is approximately 107 feet high. The embankment is approximately 6,600 feet long and is classified under the New Mexico Administrative Code (NMAC) as "intermediate" size and "significant" hazard potential. The impoundment is lined with a single HDPE geomembrane. The nominal (lowest) crest elevation (EL) is 5280.0 feet. The maximum operating water level is EL 5275.2 feet and the water level was observed to be at approximate EL 5274.2 feet during the inspection.

# **3.2 LINED DECANT WATER POND (LDWP)**

The LDWP is represented on Figure 2 – Lined Decant Water Pond (LDWP).

The LDWP (NMOSE dam number D-635) was constructed in 2003, has a maximum storage capacity of 435 acre-feet, and has a statutory height of approximately 16 feet (the LDWP was constructed on top of Ash Pond 3 and is 90 feet above the original ground surface along the South and West Embankments). The embankment is approximately 5,488 feet long and is classified under the NMAC as "intermediate" size and "significant" hazard. The impoundment is lined with two HDPE geomembranes and a leak detection layer. The maximum surcharge reservoir level is EL 5213.2 feet and the reservoir level was observed to be at approximate EL 5206.8 feet during the inspection.

# **3.3 COMBINED WASTE TREATMENT POND (CWTP)**

The CWTP is represented on Figure 3 – Combined Waste Treatment Pond (CWTP).

The CWTP is an approximately 13.4-acre unlined detention pond located adjacent to Morgan Lake. The CWTP is not regulated by NMOSE. It was constructed in 1978, has a maximum storage capacity of 137 acre-feet, and is approximately 32 feet high (maximum). The embankment is approximately 1,800 feet long and is classified under the NMAC as "small" size and "low" hazard. The CWTP is used as a settling basin for ash-transport wastewater prior to discharge to Morgan Lake through a monitored National Pollutant Discharge Elimination System (NPDES) permitted discharge point. The primary source of water entering the CWTP is from bottom ash recovery and transport processes at Units 4 and 5. Bottom ash is hydraulically transported to the Units 4 and 5 hydrobins where the transport water is separated and conveyed to the CWTP. Ash and other sediment settle in separate earthen settling basins within the CWTP footprint prior to the water overflowing into the main CWTP.

# **3.4 UPPER RETENTION SUMP**

The Upper Retention Sump (URS) is represented on Figure 4 – Upper Retention Sump.

The URS is an approximately 1.09-acre, unlined surge pond associated with operation of the flue gas desulfurization (FGD) systems for treatment of flue gas from Units 4 and 5. The URS is not regulated by NMOSE. Lime slurry is transferred from the URS into various FGD absorber vessels as needed to operate and maintain the overall FGD system.

In Spring 2018, APS started alternative management for storage of the CCR to permit the decommissioning of the existing URS and replace it with the new Upper Retention Sump Tank, a reinforced concrete tank designed to comply with regulations in 40 CFR Part 257 (EPA 2015). Upon completion, the new Upper Retention Sump Tank will replace the function of the existing Upper Retention Sump and the pipes draining into the existing Upper Retention Sump will be rerouted to the new Upper Retention Sump Tank. The existing Upper Retention Sump will then be removed from service and no longer function as a CCR unit. The Upper Retention Sump Tank will not be subject to annual inspections under the CCR Rule (EPA 2015). APS intends to refer to the new Upper Retention Sump Tank as the "Upper Retention Sump" in the future.

# **3.5 DRY FLY ASH DISPOSAL AREA (DFADA)**

The DFADA is represented on Figure 5 – Dry Fly Ash Disposal Area (DFADA).

The DFADA is a lined landfill and dry fly ash disposal facility. The DFADA currently consists of three conjoined cells: Sites 1, 2, and 3. Construction at the three Sites has been ongoing since 2007. The DFADA has a maximum intended capacity of 6,261 acre-feet and an ultimate maximum height of approximately 105 feet. Site 1 is constructed with an HDPE geomembrane overlying a compacted clay subgrade. Sites 2 and 3 are constructed with a composite liner system selected for general compliance with the EPA's *Guide for Industrial Waste Management*: a geosynthetic clay liner (GCL) overlain by an HDPE geomembrane. A drainage layer was installed over the HDPE geomembrane in all three cells as recommended in the EPA guidance. Each cell is connected to a leachate collection system designed to remove water from the storage area. The leachate collection system generally consists of a drainage layer, collection piping, a removal system, and a protective filter layer.

# 4.0 FIELD INSPECTIONS

This section contains the 2017 annual field inspections conducted by APS and accompanied by a representative from AECOM at the LAI (Section 4.1), the LDWP (Section 4.2), the CWTP (Section 4.3), the Upper Retention Sump (Section 4.4), and the DFADA (Section 4.5).

# 4.1 APS FIELD INSPECTION – LINED ASH IMPOUNDMENT (LAI)

Lined Ash Impo	undment (LAI)	State Iden	ntification Number	(SID	): D	<b>)-63</b>	4		
SID: <b>D-634</b>	Dam Name: Lined Ash Impoundment (LAI)	Type: Zoned earth and ash fill with geomembrane	Purpose: Fly ash and FGD sludge disposal						
Contact(s): Byron Conrad, P.F	E. (APS)	Report Date: January 11, 20	19						
Inspected by:Byron Conrad, P. Lee Wright, P.E.		Inspection Date: October 25,	2018						
Reviewed by: Byron Conrad, H	P.E. (APS)	Review Date: January 8, 201	19						
Design Dam Crest Elevation (ft)	): 5,280	Design Spillway Crest Elevat (rim of 8-foot-diameter rise							
Design Total Freeboard (ft): 4.	8 (West Embankment)	Measured Total Freeboard (ft <b>Corner)</b>	): 12 (in the Southwest						
Statutory Dam Height (ft): 107 (	(South Embankment)	Structural Height (ft): 107 (Se	outh Embankment)	Not Ap	7	Y	Mon Ye	Repair	Inve
Dam Crest Length (ft): 6,600		Upstream Slope: 3:1 (West Embankment) 2:1 (South Embankment)	Downstream Slope: 3:1 (West Embankment) 2:1 (South Embankment)	Not Applicable	No	'es	Monitor Yes		Investigate
Dam Crest Width (ft): 30 (Wes		Lat: <b>36° 41' 05''</b> (per NMOSE permit)	Water Rights: N/A						
20 (Sout	h Embankment)	Long: 108° 30' 26" (per NMOSE permit)	water Rights. IV/A						
Reservoir Area (acres): 126.8 (h	igh water line)	Reservoir Storage (ac-ft): 5, 5,	346 (high water line) 986 (maximum)						
Inflow Design Flood/Safe Flood	-Passing Capacity: <b>PMF</b> – f	ully contained							
Reservoir Level During Inspecti	ton (ft): EL 5274.2	Dhotoe: Vas	Dogos: <b>5</b>						
Estimated Solids Level (ft): ~ E	L 5275	– Photos: Yes	Pages: 5						

	Lined Ash Impound	ment (LAI)	SID: <b>D-634</b>	N/A	No	Yes	Mon	Rep	Inv
		CO	OMPLIANCE CHECKLIST						
1	<b>CONDITION SUMMARY, LICE</b>	ENSE, EAP, NEXT INSP	ECTION						
а	Recorded downstream hazard:	Significant	Should hazard be revised?		Χ				
b	If high hazard, estimate downstrea (PAR): N/A	am persons-at-risk	Is there a significant increase since the last inspection?		X				
c	Recorded size:	Intermediate	Should size be revised?		Χ				
d	Any safety deficiencies?	No	Describe:		Χ				
e	Any statute or rule violations?	No	Describe and list required action:		Χ				
f	Safe storage level on License:	5,275.2 feet	Should level be revised:		Χ				
g	Any License violations?	No	Describe and list required action:		Χ				
h	Date of current License:	October 27, 2015	Should new License be issued?		Х				
i	Date of last Emergency Action Pl	an revision: 2/2017	Should EAP be revised?		Χ				
j	Any Agency actions?	No	Describe and list required action:		Х				
k	Normal inspection frequency:	Weekly, Annually	Should inspection frequency be revised?		Χ				
1	Recommended date for next inspe	ection: October 2019	•	-	-	-	-		

		M	ONITORING CHECKLIST						
2	INSTRUMENTATION AND M	ONITORING							
	West Embankm	nt							
			re piezometers each (varying elevations),						
	2) Four b	ried settlement rods to n	neasure settlement at depth,						
	3) Two in	linometers, and							
	4) Two crest survey/settlement monuments.								
	North Toe Buttress								
а	Describe: 1) Eleven	lusters of three vibrating	g wire piezometers and one cluster of two vibrating wire	e piezo	meter	s (var	ying		
	elevatio	18),							
	2) Eight b	ried settlement rods to r	neasure settlement at depth, and						
	3) Three i	clinometers.							
	Other								
	1) Perman	ent water elevation mark	xers on the geomembrane liner at three locations within	the im	poun	dment	•		
	2) No infl	w or outflow measureme	ent devices.						
b	Any repair or replacement required?     No.     Describe:     X								
c	bate of last monitoring report:     January 2018 (for 2017)     Should new readings be taken and new report provided? Monthly measurement and annual reporting are required.     X								

DAM EMBANKMENT CHECKLIST					
DAM CREST					
Settlements, slides, depressions?	X				
Misalignment?	X				
Longitudinal/Transverse cracking?	X				
Animal burrows?	X				
Adverse vegetation?	X				
Erosion?	X				
	DAM CREST         Settlements, slides, depressions?         Misalignment?         Longitudinal/Transverse cracking?         Animal burrows?         Adverse vegetation?	DAM CREST         Settlements, slides, depressions?       X         Misalignment?       X         Longitudinal/Transverse cracking?       X         Animal burrows?       X         Adverse vegetation?       X	DAM CRESTSettlements, slides, depressions?XMisalignment?XLongitudinal/Transverse cracking?XAnimal burrows?XAdverse vegetation?X	DAM CRESTSettlements, slides, depressions?XMisalignment?XLongitudinal/Transverse cracking?XAnimal burrows?XAdverse vegetation?X	Settlements, slides, depressions?XXIMisalignment?XIILongitudinal/Transverse cracking?XIIAnimal burrows?XIIAdverse vegetation?XII

	Lined Ash Impoundment (LAI)	SID: <b>D-634</b>	N/A	No	Yes	Mon	Rep	Inv
4	UPSTREAM SLOPE				1	1	<u>.                                    </u>	-
а	Erosion? Yes. See of	comment i.		[	Χ		Χ	Χ
b	Inadequate ground cover?			Χ				
c	Adverse vegetation?			Х				
d	Longitudinal/Transverse cracking? Could not	t observe due to the presence of the geomembrane liner.	Χ					
e	Inadequate riprap? The upstr	eam slope is covered with a geomembrane liner.	Χ					
f	Stone deterioration?		Χ					
g	Settlements, slides, depressions, bulges? See comm	nent ii.			Χ		Χ	Χ
h	Animal burrows?			Χ				
5	DOWNSTREAM SLOPE							
а	Erosion? See comment iv.				Χ	Χ		
b	Inadequate ground cover? sporadic and uneven v	slopes are faced with bottom ash that supports only egetation. A lime-based, white- and turquoise-colored dust pplied in accordance with the Plant's Dust Control Plan.		x				
c	Adverse vegetation?			Χ				
d	Longitudinal/Transverse cracking?			X				
e	Inadequate riprap?		Χ					
f	Stone deterioration?		Χ					
g	Settlements, slides, depressions, bulges?			Χ				
h	Soft spots or boggy areas?			Χ				
i	Movement at or beyond toe?			Χ				
j	Animal burrows?			Χ				
6	ABUTMENT CONTACTS							
a	Erosion?			Х				
b	Differential movement?			Χ				
c	Cracks?			Χ				
d	Settlements, slides, depressions, bulges?			Χ				
e	Seepage?			Χ				
f	Animal burrows?			Χ				

7	SEEPAGE/PIPING CONTI	ROL DESIGN FEATURE(S)						
а	Describe:	Historic seepage at the downstream toe of the South Embankment is captured using toe. There was no flow from the outlet at the time of inspection (photo IMG_1415).	g a Fr	ench	drain	benea	th the	<u>}</u>
b	Internal drains flowing?	APS is currently pumping water out of the Southwest Corner and into the Drop Inlet Structure.			X			
с	Seepage at or beyond toe?			Χ				
d	If so, does seepage contain fi	nes?	Χ					
e	Evidence of sand boils at or	beyond toe?		Χ				

		RESERVOIR CHECKLIST				
8	RESERVOIR					
а	High water marks?			Х		
b	Erosion/slides into pool area?		X			
с	Sediment accumulation?	Suspended FGD solids and fly ash settle in the impoundment.		Х		
d	Floating debris present?	Sparse debris on top of the impounded ash.	X			
e	Depressions, sinkholes, or vortices?		X			
f	Low ridges/saddles allowing overflow?		X			
g	Structures below dam crest elevation?	Yes. See comment vii.		Χ		

#### Additional comments and recommendations for the LAI:

- During the inspection, four rectangular holes in the geomembrane liner were observed i. along the South Embankment below the impounded water level (Photos IMG 1227 and IMG 1386). The straight edges along each hole suggests the holes were cut intentionally (compare Photo IMG 1229 and IMG 1235 in Appendix A of this Inspection Report with Photo IMG 5216 and IMG 5228 in Appendix A of the 2017 Inspection Report). One of the holes appeared to be draining water from underneath the geomembrane liner at the time of the inspection, but the three other holes appeared to be allowing the upstream clay blanket to erode into the impoundment. All of the holes in the geomembrane liner should be repaired as soon as it can be safely done and the purpose for creating the holes should be investigated. The LAI embankment was designed to be stable without the geomembrane liner (URS Corporation 2012); however, the upstream slope and the toe drain along the South Embankment should be monitored for evidence of internal erosion. Evidence could include benching along the upstream slope due to the erosive action of water against the clay and cloudy seepage flowing out of the toe drain. The South Embankment toe drain was dry on the date of this inspection (photo IMG 1415). APS does not believe that the presence of water beneath the liner, nor the damage to the liner itself presents a safety concern since the LAI was designed to be stable without the presence of the liner.
- ii. A depression (Photo IMG\_1233) and two bulges (Photo IMG\_1244) were observed along the upstream slope in the Southwest Corner of the impoundment. These features are near the holes, trapped water, and erosion described in comment i and may be related. The causes of the depression and bulges should be investigated and these features should be repaired.
- iii. Recent upgrades to the selective catalytic reduction system in the Plant adversely affected the FGD system chemistry and required APS to use more water than normal. This additional water was eventually sent to the LAI, where it flowed to the Southwest Corner of the impoundment. APS is currently pumping this water from the LAI to the LDWP to reuse in the Plant the FGD system chemistry. The water is being pumped from the Southwest Corner to the Drop Inlet Structure via a single-walled HDPE pipe placed along the crest of the impoundment and placed on top of the liner. In the meantime, APS's CCR hauling contractor who operates this pump is instructed to run the pump on the daylight shift only and monitor the HDPE pipe.
- iv. The downstream slopes of the West Embankment and the Northwest Embankment have minor erosion rills (Photos IMG\_1269, IMG\_1017, and IMG\_1338). Continue monitoring erosion features and repair them if the erosion depth exceeds 1 foot.
- v. There are small tears and holes in the liner along the crest of the East Embankment (Photos IMG\_1358, IMG\_1373, and IMG\_1375). The tears should be repaired to prevent stormwater or other runoff from entering the space beneath the liner.
- vi. The North Toe Buttress (NTB) was constructed as part of the 5280 Lift of the LAI to provide additional stability in the northern portion of the West Embankment (photo

IMG\_1294). The NTB appeared to be in good condition during the inspection. The NTB foundation instruments indicate normal, expected foundation conditions.

- vii. The primary outlet from the LAI is an 8-foot diameter vertical, perforated HDPE riser connected at the bottom to 16-inch and 8-inch diameter HDPE gravity pipe outlets that drain into the LDWP.
- viii. The weekly inspection reports for the period between October 1, 2017 and September 30, 2018 indicate the following:
  - a. Signs of erosion requiring repair were observed on the dam crest and downstream slope on October 5, 2017. APS proceeded to repair the affected areas.
  - ix. The weekly inspection reports do not indicate that there were any appearances of actual or potential structural weakness or other conditions that have the potential to disrupt the operation or safety of the CCR unit.

# 4.2 APS FIELD INSPECTION – LINED DECANT WATER POND (LDWP)

Lined Decant V	Water Pond (LDWI	P)	State	Identification Nun	nber	(SI	<b>D):</b> ]	D-6	35	
SID: <b>D-635</b>	Dam Name: Lined Decant Water Pond (LDWP)	ash fill wit	ed earth and th double-liner rane and leak	Purpose: Store recycled LAI decant water and collected groundwater						
Contact(s): Byron Conrad, P.E.	(APS)	Report Dat	te: January 11, 2	019						
Inspected by:Byron Conrad, P.E. Lee Wright, P.E. (A		Inspection	Date: October 25	5, 2018						
Reviewed by: Byron Conrad, P.F	E. (APS)	Review Da	ate: January 9, 20	)19						
Design Dam Crest Elevation (ft): 5	5,216	Design Spi	illway Crest Eleva	ation: No spillway						
Design Total Freeboard (ft): 2.8 ( surc	above the maximum harge level, EL 5213.2)	Measured	Total Freeboard (	ft): <b>9.2</b>			Monitor Yes			
Statutory Dam Height (ft): 16		Structural	Height (ft): 16		Not Applicable	No		Moni	Repair	Investigate
Dam Crest Length (ft): 5,488		Upstream	Slope: 3:1	Downstream Slope: 2:1	licable			Monitor	ur <sup>.</sup>	gate
Dam Crest Width (ft): 30 feet (No	orth, East Embankments)	Lat: 36° 41 (per NMO	l' 00" OSE permit)	Watar Dichta: N/A						
20 feet (W	est, South Embankments)	Long: 108 <sup>o</sup> (per NMO	° 30' 45'' )SE permit)	Water Rights: N/A						
Reservoir Area (acres): 45.4 (at E per APS	EL 5213.2 ft) drawing 150793.2.1	Reservoir		5 (normal operating pacity)						
Inflow Design Flood/Safe Flood-P	Passing Capacity: <b>PMF – fully</b>	contained								
Reservoir Level During Inspection	n (ft): ~ EL 5206.8			D 4						
Estimated Solids Level (ft): N/A ( impound a significant volume of		- Photos: Ye	es	Pages: 4						

J	Lined Decant Water <b>F</b>	Pond (LDWP)	SID: <b>D-635</b>	N/A	No	Yes	Mon	Rep	Inv
		СС	OMPLIANCE CHECKLIST						
1	<b>CONDITION SUMMARY, LICE</b>	ENSE, EAP, NEXT INSP	ECTION						
а	Recorded downstream hazard:	Significant	Should hazard be revised?		Χ				
b	If high hazard, estimate downstrea (PAR): N/A	am persons-at-risk	Is there a significant increase since the last inspection?		X				
c	Recorded size:	Intermediate	Should size be revised?		Χ				
d	Any safety deficiencies?	No	Describe:		Χ				
e	Any statute or rule violations?	No	Describe and list required action:		Χ				
f	Safe storage level on License:	5,213.2 feet	Should level be revised:		Χ				
g	Any License violations?	No	Describe and list required action:		Χ				
h	Date of current License:	February 7, 2008	Should new License be issued?		Χ				
i	Date of last Emergency Action Pl	an revision: 2/2017	Should EAP be revised?		Χ				
j	Any Agency actions?	No	Describe and list required action:		Χ				
k	Normal inspection frequency:	Weekly, Annually	Should inspection frequency be revised?		Χ				
1	Recommended date for next inspe	ection: October 2019	•	•	•	•	•		

		М	ONITORING CHECKLIST				
2	INSTRUMENTATION AND MONITO	RING					
	Instrumentation:						
	1) Eight standpipe	e piezometers					
	2) Two crest surve	ey/settlement monu	uments.				
	Describe: Other						
а	1) Interstitial geom	tection and evacuation pump.					
	2) Surveyed level i	markings on geom	embrane liner.				
	3) No inflow meas	urement devices.					
	4) Outflow estimat	tion by LDWP pur	mp rating/hours of operation, if needed.				
b	Any repair or replacement required?	No.	Describe:	Χ			
		1	Should new readings be taken and new report				
с	Date of last monitoring report.	January 2018 (for 2017)	provided? Monthly measurement and annual		Χ		
		$(101 \ 201 \ )$	reporting are required.				

	DAM EMBANKMENT CHECKLIST										
3	DAM CREST										
а	Settlements, slides, depressions?			Χ							
b	Misalignment?			Χ							
c	Longitudinal/Transverse cracking?			Χ							
d	Animal burrows?			Χ							
e	Adverse vegetation?			Χ							
f	Erosion?			Χ							
4	UPSTREAM SLOPE										
а	Erosion? The up	stream slope is covered with geomembrane.		Χ							
b	Inadequate ground cover?			Χ							
с	Adverse vegetation?			Χ							
d	Longitudinal/Transverse cracking? Could r	ot observe due to the presence of the geomembrane liner.	Х								
e	Inadequate riprap?		Χ								
f	Stone deterioration?		Х								
g	Settlements, slides, depressions, bulges?			X							
h	Animal burrows?			Χ							

]	Lined Decant Water	r Pond (LDWP)	SID: <b>D-635</b>	N/A	No	Yes	Mon	Rep	Inv
5	DOWNSTREAM SLOPE								
а	Erosion?	Minor rilling on the West an	nd North Embankments.			Χ	Χ		
b	Inadequate ground cover?	supports only sporadic and	Embankment slopes are faced with bottom ash that uneven vegetation. A lime-based, white- and pression agent is applied in accordance with the		X				
c	Adverse vegetation?				Χ				
d	Longitudinal/Transverse crack	king?			Χ				
e	Inadequate riprap?			Χ					
f	Stone deterioration?			Χ					
g	Settlements, slides, depression	ns, bulges? Yes. See comm	nent ii.			Χ		Χ	
h	Soft spots or boggy areas?								
i	Movement at or beyond toe?								
j	Animal burrows?								
6	ABUTMENT CONTACTS								
а	Erosion?				Χ				
b	Differential movement?				Χ				
c	Cracks?				Χ				
d	Settlements, slides, depression	ns, bulges?			Χ				
e	Seepage?				Χ				
f	Animal burrows?				Χ				
7	SEEPAGE/PIPING CONTRO	OL DESIGN FEATURE(S)							
а	Describe: All pump	os and pumping systems app	eared to be functioning at the time of the inspection.		Χ				
b	Internal drains flowing?					Χ			
с	Seepage at or beyond toe?				Χ				
d	If so, does seepage contain fin	les?		Χ					
e	Evidence of sand boils at or be	eyond toe?			Χ				

	RESERVOIR CHECKLIST										
8	RESERVOIR										
a	High water marks?			Χ							
b	Erosion/slides into pool area?		X								
c	Sediment accumulation?	Minor amounts of suspended FGD solids and fly ash may settle in the impoundment.		X							
d	Floating debris present?		X								
e	Depressions, sinkholes, or vortices?		X								
f	Low ridges/saddles allowing overflow?		X								
g	Structures below dam crest elevation?	The interstitial geomembrane leak detection and evacuation pump system includes a pump situated between the two geomembrane liners. See comment iii.		x							

#### Additional comments and recommendations for the LDWP:

- i. Shallow erosion rills observed on the North and West Embankments during the inspection should be monitored and repaired if they are observed to exceed 1 foot in depth.
- ii. Two shallow sloughs were observed on the lowermost bench of the West Embankment (Photos IMG\_1435 and IMG\_1438). The sloughs are laterally extensive and should be repaired.
- iii. The LDWP interstitial geomembrane leak detection and evacuation pump was operating at the time of the inspection (Photos IMG\_1463 and IMG\_1471). Because of the water chemistry in the LDWP, the commercially available, submersible pumps break down on a regular basis. APS has determined that regularly replacing the pumps is more economical and feasible than temporarily decommissioning the entire pond and constructing a different access port configuration. Because the pump is replaced on a regular basis, the Plant should continue to monitor the system for signs the pump has or is about to break down.
- iv. There were several dents, holes, and tears in the liner along the South, North, and East Embankments (Photos IMG\_1521, IMG\_1529, IMG\_1530, IMG\_1571, and IMG\_1572). Some of the damaged areas were also observed during the 2017 inspection. Damage to the liner should be repaired and the liner should be monitored for additional tears and cuts.
- v. The liner was observed to be pulling out of the anchor trench in isolated areas along the West and East Embankments (Photos IMG\_1510 and IMG\_1564). The liner was observed to be pulling out of the anchor trench in this area during the 2017 inspection as well.
- vi. The 7-day inspection reports for the period between October 1, 2017 and September 30, 2018 do not indicate that there were any appearances of actual or potential structural weakness or other conditions which have the potential to disrupt the operation or safety of the CCR unit.

# 4.3 APS FIELD INSPECTION – COMBINED WASTE TREATMENT POND (CWTP)

Combined Was	<b>Combined Waste Treatment Pond (CWTP)</b> State Identification							D): N	I/A	
SID: N/A	Dam Name: Combined Waste Treatment Pond (CWTP)	Type: Earth	I	Purpose: CCR-transport surface water collection						
Contact(s): Byron Conrad, P	.E. (APS)	Report Date: Jar	10 nuary 11, 20	019						
Inspected by: Byron Conrad, Lee Wright, P.E		Inspection Date:	October 24	l, 2018						
Reviewed by: Byron Conrad,	P.E. (APS)	Review Date: January 9, 2019								
Design Dam Crest Elevation (	ft): <b>5,335</b>	Design Spillway Crest Elevation (ft): <b>5,328.77</b>								
Design Total Freeboard (ft): 7		Measured Total Freeboard (ft): Not measured								
Statutory Dam Height (ft): 32 (max), 22.81 (avg)		Structural Height (ft): 32 (max), 22.81 (avg)		Not Applicable	No	Yes	Monitor	Repair	Investigate	
Dam Crest Length (ft): 1,800		Upstream Slope:	2:1	Downstream Slope: 1.5:1	plicable	0	es	nitor	oair	tigate
Dom Graat Width (ft): 24 20		Lat: 34° 41′ 29.1	9″N	Water Dichter N/A						
Dam Crest Width (ft): 24-30		Long: 108° 28' 2	28.73″W	Water Rights: N/A						
Reservoir Area (acres): 13.4 ( for decant cells)	7.5 acres for reservoir, 5.9 acres	Reservoir Storag stormwater stor		7 (27 additional ac-ft for						
Inflow Design Flood/Safe Flood-Passing Capacity: Not Calculated										
Reservoir Level During Inspection (ft): ~EL 5329 (water was passing over the spillway)		Dhoton V		Dages: 4						
	ariable (below EL 5328.77). The ed to remove impounded solids.	Photos: Yes		Pages: 4						

	Combined Waste Trea (CWTP)	atment Pond	SID: N/A	N/A	No	Yes	Mon	Rep	Inv
		CC	OMPLIANCE CHECKLIST						
1	<b>CONDITION SUMMARY, LICE</b>	NSE, EAP, NEXT INSP	ECTION						
a	Recorded downstream hazard:	Low	Should hazard be revised?		Χ				
b	If high hazard, estimate downstreat (PAR): N/A	m persons-at-risk	Is there a significant increase since the last inspection?		X				
c	Recorded size:	Small	Should size be revised?		Χ				
d	Any safety deficiencies?	No	Describe:		Χ				
e	Any statute or rule violations?	No	Describe and list required action:		Χ				
f	Safe storage level on License:	N/A	Should level be revised:		Χ				
g	Any License violations?	No	Describe and list required action:		Χ				
h	Date of current License:	N/A	Should new License be issued?		Χ				
i	Date of last Emergency Action Pla	n revision: N/A	Should EAP be revised?		Χ				
j	Any Agency actions?	No	Describe and list required action:		Χ				
k	Normal inspection frequency:	Weekly, Annually	Should inspection frequency be revised?		Χ				
1	Recommended date for next inspec	ction: October 2019							

	MONITORING CHECKLIST												
2	INSTRUMENTATION AND MO	NITORING											
а	Describe: There are four monitoring wells for this structure to comply with groundwater monitoring requirements.												
b	Any repair or replacement required? N/A		Describe: N/A		X								
с	Date of last monitoring report:	January 2018 (for 2017)	Should new readings be taken and new report provided? <b>Annual reporting is required.</b>			X							

#### DAM EMBANKMENT CHECKLIST

3	DAM CREST						
a	Settlements, slides, depressions?	The crest appeared to be flat (with a slight grade to the upstream side) and in good condition.		X			
b	Misalignment?			Χ			
с	Longitudinal/Transverse cracking?			Χ			
d	Animal burrows?	None observed. The road is graded regularly. Continue to monitor.		Χ		Χ	
e	Adverse vegetation?	None observed. The road is graded regularly.		Χ			
f	Erosion?	Two shallow erosion holes were observed on the upstream shoulder (Photo IMG_0931). Repair and monitor the area.			X	X	
4	UPSTREAM SLOPE						
a	Erosion?	See comment i.			Χ	Χ	
b	Inadequate ground cover?			Χ			
c	Adverse vegetation?	Vegetation on the upstream slope generally consists of tall grasses in the middle and eastern portion of the embankment.		x			
d	Longitudinal/Transverse cracking?			Χ			
e	Inadequate riprap?	No riprap was observed above the water line on the upstream slope.			Х		
f	Stone deterioration?		Χ				
g	Settlements, slides, depressions, bulge	Portions of the slope are steeper than others (Photo IMG_0961).			Χ		
h	Animal burrows?	None observed. Continue to monitor.		Χ		Χ	

	Combined Waste Treatme (CWTP)	nt Pond	SID: N/A	N/A	No	Yes	Mon	Rep	Inv
5	DOWNSTREAM SLOPE								
а	Erosion?	See comment i	ii.			X	X		
b	Inadequate ground cover?				Χ				
c	Adverse vegetation?	Isolated instan IMG_0914, an	nces of adverse vegetation (Photos IMG_0909, d IMG_0921).			X	x		
d	Longitudinal/Transverse cracking?	See comment i	v.			X	X		
e	Inadequate riprap?	See comment v	V.		Χ				
f	Stone deterioration?				Χ				
g	Settlements, slides, depressions, bulges?	See comments	iii and iv.			Х	Х		
h	Soft spots or boggy areas?				X				
i	Movement at or beyond toe?	Cannot observ	/e.	Χ					
j	Animal burrows?	None observed	l. Continue to monitor.		Χ		X		
6	ABUTMENT CONTACTS								
а	Erosion?				Χ				
b	Differential movement?				Χ				
c	Cracks?				Χ				
d	Settlements, slides, depressions, bulges?				Χ				
e	Seepage?				Χ				
f	Animal burrows?	None observed	l. Continue to monitor.		Χ		Χ		
7	SEEPAGE/PIPING CONTROL DESIGN	V FEATURE(S)							
а	Describe:	None.							
b	Internal drains flowing?			Χ					
с	Seepage at or beyond toe?	Cannot observ	/e.	Χ					
d	If so, does seepage contain fines?			X					
e	Evidence of sand boils at or beyond toe?			X					

	RESERVOIR CHECKLIST										
8	RESERVOIR										
a	High water marks?			X							
b	Erosion/slides into pool area?			X							
c	Sediment accumulation?	See comment vi.			X						
d	Floating debris present?			X							
e	Depressions, sinkholes, or vortices?			X							
f	Low ridges/saddles allowing overflow?	A weir allows overflow into the NPDES outlet.			X						
g	Structures below dam crest elevation?	Twin 30-inch reinforced concrete pipe outlets are located at the eastern side of the CWTP.			X						

Additional comments and recommendations for the CWTP:

- i. The irregular erosion along the upstream slope (Photo IMG\_0961) appeared to be unchanged compared to previous inspections. Continue to monitor the area.
- ii. Minor vegetation (grass, small trees, and shrubs) was observed on the slopes during this inspection (photos IMG\_0909, IMG\_0914, and IMG\_0921). Continue monitoring vegetation in accordance with the NMOSE vegetation maintenance guidelines "*Vegetation Management on Dams*" (2011). The woody vegetation on the upstream slope (Photo IMG\_0952) should be repaired if needed using the NMOSE vegetation management guidelines (NMOSE 2011).
- iii. Several instances of minor erosion were observed on the downstream slope above the riprap (Photos IMG\_0913 and IMG\_0927). These areas should be monitored and repaired if the erosion depth exceeds one foot.
- iv. A series of incipient longitudinal cracks was observed along the downstream slope above the riprap and water line (Photo IMG\_0933). It was not clear during the inspection if the cracks would result in a shallow slough or deeper-seated failure. The area should be monitored and repaired if the cracks expand in depth or extent.
- v. APS installed additional riprap on the downstream slope of the embankment in August 2017 to prevent wave erosion along the slope (photo IMG\_0915). The additional riprap was placed from approximately 5 feet below the canal water surface to approximately 2 feet above the canal water surface.
- vi. The facility includes seven decant cells and one forebay cell in the western half of the CWTP. Flow from the collection distribution vault is directed to the selected cells. Settled solids are periodically removed and decanted water flows to the CWTP free water pond. Suspended sediment and CCR settle in the decant cells in the western half of the impoundment.
- vii. The HDPE pipe observed laying across the upstream slope during previous inspections was not observed during this inspection.
- viii. The 7-day inspection reports for the period between October 1, 2017 and September 30, 2018 do not indicate that there were any appearances of actual or potential structural weakness or other conditions which have the potential to disrupt the operation or safety of the CCR unit.

# 4.4 APS FIELD INSPECTION – UPPER RETENTION SUMP

Upper Retention	Upper Retention Sump		State Identification Number (SID): N/A								
SID: N/A	Dam Name: Upper Retention Sump	Type: Incised	Purpose: CCR-transport surface water collection								
Contact(s): Byron Conrad, P.E. (APS)		Report Date: January 11, 2	2019								
Inspected by: Byron Conrad, P.E. (APS Lee Wright, P.E. (AECO)		Inspection Date: October 2	24, 2018								
Reviewed by: Byron Conrad, P.E. (APS	5)	Review Date: January 9, 2	019								
Design Dam Crest Elevation (ft): 5,350.5	;	Design Spillway Crest Elevation: None									
Design Total Freeboard (ft): 6.5		Measured Total Freeboard (ft): ~11.25									
Statutory Dam Height (ft): 0 (incised)	Statutory Dam Height (ft): 0 (incised)		Structural Height (ft): 0 (incised)		No	Yes	Monitor	Repair	Investigate		
Dam Crest Length (ft): 900 (approx.)		Upstream Slope: 2:1	Downstream Slope: N/A	Not Applicable	0	es	nitor	oair	tigate		
Dam Crest Width (ft): Varies		Lat: <b>36°41'14.26''N</b>	- Water Rights: N/A								
Dam Crest width (it). Varies		Long: 108°28'37.91''W	water Rights. IV/A								
Reservoir Area (acres): 1.09 (nominal –	Reservoir Area (acres): 1.09 (nominal – see comment i) Reservoir Storage (ac-ft): 10.7 (nominal – see comment i)										
Inflow Design Flood/Safe Flood-Passing Capacity: Not Calculated											
Reservoir Level During Inspection (ft): ~	EL 5339.25	Photos: <b>Yes</b>	Pages: 4								
Estimated Solids Level (ft): ~ EL 5339.2	5		Pages: 4								

	Upper Retention	ı Sump	SID: N/A	N/A	No	Yes	Mon	Rep	Inv
		С	OMPLIANCE CHECKLIST						
1	<b>CONDITION SUMMARY, LICE</b>	NSE, EAP, NEXT INSP	ECTION						
а	Recorded downstream hazard:	Very Low	Should hazard be revised?		Х				
b	If high hazard, estimate downstrea (PAR): N/A	m persons-at-risk	Is there a significant increase since the last inspection?		X				
с	Recorded size:	Small	Should size be revised?		Х				
d	Any safety deficiencies?	No	Describe:		Х				
e	Any statute or rule violations?	No	Describe and list required action:		Χ				
f	Safe storage level on License:	N/A	Should level be revised:		Χ				
g	Any License violations?	No	Describe and list required action:		Х				
h	Date of current License:	N/A	Should new License be issued?		Χ				
i	Date of last Emergency Action Pla	n revision: N/A	Should EAP be revised?		Χ				
j	Any Agency actions?	No	Describe and list required action:		Χ				
k	Normal inspection frequency:	Weekly, Annually	Should inspection frequency be revised?			Χ			
1	Recommended date for next inspe-	ction: See comment							

	MONITORING CHECKLIST												
2	INSTRUMENTATION AND MONITORING												
а	Describe: There are no instruments or other monitoring devices for this structure due to its small size.												
b	Any repair or replacement required? N/A Describe: N/A				Χ								
c	Date of last monitoring report:	January 2018 (for 2017)	Should new readings be taken and new report provided? N/A		X								

	DAM EMBANKMENT CHECKLIST					
3	DAM CREST					
а	Settlements, slides, depressions?		X			
b	Misalignment?		X			
c	Longitudinal/Transverse cracking	?	X			
d	Animal burrows?		X			
e	Adverse vegetation?		X			
f	Erosion?		X			
4	UPSTREAM SLOPE					
а	Erosion?	The remaining active portion of the Upper Retention Sump is lined with soil cement.	X			
b	Inadequate ground cover?		X			
с	Adverse vegetation?		X			
d	Longitudinal/Transverse cracking	?	X			
e	Inadequate riprap?		X			
f	Stone deterioration?	Most of the soil cement facing has been removed due to construction.	X			
g	Settlements, slides, depressions, b	oulges?	X			
h	Animal burrows?		X			

	Upper Retention Sump	SID: N/A	N/A	No	Yes	Mon	Rep	Inv
5	DOWNSTREAM SLOPE		<b>I</b>			<u>.                                    </u>		
а	Erosion? There is no downstream slo	pe.	Х					
b	Inadequate ground cover?		Х					
c	Adverse vegetation?		Х					
d	Longitudinal/Transverse cracking?		X					
e	Inadequate riprap?		Х					
f	Stone deterioration?		X					
g	Settlements, slides, depressions, bulges?		Х					
h	Soft spots or boggy areas?							
i	Movement at or beyond toe?							
j	Animal burrows?							
6	ABUTMENT CONTACTS							
а	Erosion? There are no abutments for	• the incised CCR Unit.	X					
b	Differential movement?		X					
c	Cracks?		X					
d	Settlements, slides, depressions, bulges?		X					
e	Seepage?		X					
f	Animal burrows?		X					
7	SEEPAGE/PIPING CONTROL DESIGN FEATURE(S)							
а	Describe: None.							
b	Internal drains flowing?		X					
c	Seepage at or beyond toe? There is no downstream toe		Х					
d	If so, does seepage contain fines?		Х					
e	Evidence of sand boils at or beyond toe?		Х					

	RESERVOIR CHECKLIST								
8	RESERVOIR								
a	High water marks?			Х					
b	Erosion/slides into pool area?			Х					
c	Sediment accumulation?	See comment iii.			Х				
d	Floating debris present?			Х					
e	Depressions, sinkholes, or vortices?			Х					
f	Low ridges/saddles allowing overflo	w?		Х					
g	Structures below dam crest elevation?	Yes. There is an evacuation pump system, pump chamber, and at least two reinforced concrete inlet pipes. The evacuation pump system discharges to above-ground lines.			X				

#### Additional comments and recommendations for the Upper Retention Sump:

- i. In Spring 2018, APS began alternative management for storage of the CCR, to permit the decommissioning of the existing Upper Retention Sump and replacing it with the new Upper Retention Sump Tank to comply with regulations in 40 CFR Part 257 (EPA 2015). At the time of the inspection, construction of the new Upper Retention Sump Tank was nearly complete and the active portion of the existing Upper Retention Sump had been reduced to a fraction of its previous capacity (Photos IMG\_0850, IMG\_0866A, IMG\_0862, and IMG\_0867). Upon completion of the new Upper Retention Sump Tank construction, the existing Upper Retention Sump Tank will be removed from service and no longer function as a CCR unit.
- ii. All of the discharge pipes at various locations around the perimeter of the Upper Retention Sump have been rerouted to the south end of the site footprint. In addition, a wall has been constructed along the south end of the Upper Retention Sump to minimize the active portion of the site footprint and separate it from the new Upper Retention Sump Tank construction (Photos IMG\_0866A, IMG\_0861, and IMG\_0862).
- iii. APS has significantly decreased the volume of water and solids stored in the remaining portion of the existing Upper Retention Sump due to ongoing construction of the new Upper Retention Sump Tank.
- iv. The 7-day inspection reports for the period between October 1, 2017 and September 30, 2018 do not indicate that there were any appearances of actual or potential structural weakness or other conditions which have the potential to disrupt the operation or safety of the CCR unit.

# 4.5 APS FIELD INSPECTION – DRY FLY ASH DISPOSAL AREA (DFADA)

Dry Fly Ash Disposal Area (DFADA)		State Identification Number (SID): N/A							
SID: N/A	Landfill Name: Dry Fly Ash Disposal Area (Cells 1, 2, and 3)	Type: Lined Landfill	Purpose: Permanent storage of dry CCR (fly ash, bottom ash, dry FGD solids) and select construction debris (e.g. concrete and wood)						
Contact(s): Byron Conrad, P.E. (A	PS)	Report Date: January 11, 2	2019						
Inspected by: Byron Conrad, P.E. (APS), Lee Wright, P.E. (AECOM)		Inspection Date: October 2	4-25, 2018						
Reviewed by: Byron Conrad, P.E. (	Reviewed by: Byron Conrad, P.E. (APS)		Review Date: January 9, 2019						
Design Maximum Ash Elevation (ft): <b>5,295</b>		Current Ash Elevation (ft): Based on survey data from FHI: Cell 1 is ~ EL 5295 feet (July 2018) Cell 2 is ~ EL 5273 feet (September 2018) Cell 3 is ~ EL 5268 feet (July 2018)		Not Applicable	No	Yes	Monitor	Repair	Investigate
Dam Crest Length (ft): Not applicable		Design Side Slope: Varies. 4:1 on final outside slopes, 2:1 on internal slopes.	Observed Side Slope: Varies. 4:1 on final outside slopes, 2:1 on internal slopes.	icable		-	or	Ш <sup>.</sup>	gate
Dam Crest Width (ft): <b>Not applicable</b>		Lat: 36°40'43.27"N Long: 108°30'12.2 W	- Water Rights: N/A						
Landfill Area (acres): 94.8 (Current, Cells 1, 2, and 3)		Landfill Capacity (ac-ft): 6,261 for Cells 1, 2, and 3							
Inflow Design Flood/Safe Flood-Passing Capacity: Diversion of run-off from 25-year, 24 hour storm, spillway passage of impa									
Photos: Yes		Pages: 3							

D	ory Fly Ash Disposal Ar	ea (DFADA)	SID: N/A	N/A	No	Yes	Mon	Rep	Inv	
	MONITORING CHECKLIST									
1	INSTRUMENTATION AND MON	ITORING								
a	Describe:	There are no instrum	nents or other monitoring devices for this structure.							
b	Any repair or replacement required?	N/A	Describe: N/A		Χ					
c	Date of last monitoring report:	January 2018 (for 2017)	Should new readings be taken and new report provided? <b>Annual reporting is required.</b>			X				
2	2 CONDITION SUMMARY									
a	Waste placed in good practices?					Х				
3	LANDFILL CONFIGURATION									
a	Settlements, slides, slope stability?				Χ					
b	Cracking?				Х					
c	Run on control?					Х	Χ	Χ		
d	Run off control?					Χ				
e	Erosion?	See comment ii.			Χ		Χ			
f	Dust control issues?	See comment vii.				Χ	Χ			

Additional comments and recommendations for the DFADA:

- i. There is evidence of head-cutting at the inlet to the Stormwater Diversion Channel (Photo IMG\_1429). The affected area appears to be relatively unchanged compared to the 2015, 2016, and 2017 observations. Sediment is accumulating in the adjacent detention basin.
- ii. Erosion observed along the western toe of Cell 3 during the 2017 inspection has been repaired (Photo IMG\_0933), but there has also been additional, less significant erosion in the same place (Photo IMG\_0937). Continue to monitor this area and repair erosion channels/gullies when they exceed a depth of one foot.
- iii. Ash placement and compaction at the DFADA is in approximate 6-inch thick lifts using end dumps and with compaction applied by a tractor-pulled, smooth, static drum. CCR solids placed for landfilling appeared to be placed in accordance with the contract specifications for density control.
- Run on control The run on control system consists of a detention basin and diversion ditch to direct storm water around the DFADA. In addition to the head-cutting at the inlet, there was also significant (approximately 5 feet deep) erosion at the outlet south of Cell 1 (Photo IMG\_1422) and sediment accumulation upstream of the outlet (Photo IMG\_1423). The run on control system otherwise appears to be in good condition and the absence of excessive erosion at the toe of Cells 1 and 2 indicates that the run on control system is functioning as intended.
- v. Run off control There are no external runoff collection ditches. Internal drain systems report to two separate lined leachate cell collection ponds for Cells 1 and 2 (Photo IMG\_1246). Cell 3 drains to the Cell 1 collection pond. The water level in these two ponds is maintained by the ash haul contractor by use of a mobile suction pump. This water is utilized for dust control on site.
- vi. Several plants were observed to have taken root through holes in the Pyramat geosynthetic covering along the west side of Cell 1 (Photos IMG\_1136 and IMG\_1157).

These do not currently appear to affect the stability of the landfill, but could ultimately affect the integrity of the Pyramat.

- vii. During the inspection, there were no indications that the site was experiencing dust control issues due to wind blowing away ash placed in the landfill. However, vacuum trucks contracted to remove ash from the Plant area were observed to be allowing ash to blow across the site as it was being dumped from the truck (Photo IMG\_1130). Vacuum trucks should take more care to minimize dust when unloading ash at the site.
- viii. The 7-day inspection reports for the period between October 1, 2017 and September 30, 2018 do not indicate that there were any appearances of actual or potential structural weakness or other conditions which have the potential to disrupt the operation or safety of the CCR unit.

# 5.0 DATA REVIEW

#### 5.1 LINED ASH IMPOUNDMENT

#### 5.1.1 Geometry Changes Since Last Inspection

There have not been any significant changes to the geometry of the unit since the last inspection in 2017.

#### 5.1.2 Instrumentation

The locations of geotechnical and other related instrumentation in the vicinity of the LAI are shown on Figure 6 – Lined Ash Impoundment (LAI) Instrumentation Map.

The minimum and maximum recorded readings for each instrument over the October 1, 2017 – September 30, 2018 (current) review period are reported in the following table:

Instrument Name	Minimum	Maximum	Unit						
	LAI Piezometers (10/1/17 to 9/30/18)								
P-7.1	5196.87 <sup>1</sup>	5196.87 <sup>1</sup>	elevation head						
P-7.2	5191.35 <sup>1</sup>	5191.35 <sup>1</sup>	elevation head						
P-7.3	5184.75 <sup>1</sup>	5184.75 <sup>1</sup>	elevation head						
P-8.1	5196.60 <sup>1</sup>	5196.60 <sup>1</sup>	elevation head						
P-8.2	5182.10 <sup>1</sup>	5182.10 <sup>1</sup>	elevation head						
P-8.3	5174.10 <sup>1</sup>	5174.10 <sup>1</sup>	elevation head						
P-9.1	5196.87 <sup>1</sup>	5196.87 <sup>1</sup>	elevation head						
P-9.2	5183.97 <sup>1</sup>	5183.97 <sup>1</sup>	elevation head						
P-9.3	5170.87 <sup>1</sup>	5170.87 <sup>1</sup>	elevation head						
P-10.1	5198.22 <sup>1</sup>	5198.22 <sup>1</sup>	elevation head						
P-10.2	5184.22 <sup>1</sup>	5184.22 <sup>1</sup>	elevation head						
P-10.3	5173.72 <sup>1</sup>	5173.72 <sup>1</sup>	elevation head						
P-11.1	5200.90	5201.82	elevation head						
P-11.2	5189.65 <sup>1</sup>	5189.65 <sup>1</sup>	elevation head						
P-11.3	5174.65 <sup>1</sup>	5174.65 <sup>1</sup>	elevation head						
P-12.1	5202.54 <sup>1</sup>	5202.54 <sup>1</sup>	elevation head						
P-12.2	5186.54 <sup>1</sup>	5186.54 <sup>1</sup>	elevation head						
P-12.3	5176.54 <sup>1</sup>	5176.56	elevation head						
<sup>1</sup> Porewater	<sup>1</sup> Porewater pressure measurements are negative (draining condition)								

Instrument Name	Minimum	Maximum	Unit			
	NTB Piezometers (	10/1/17 to 9/30/18)				
P-100.1	5202.06 <sup>1</sup>	5202.06 <sup>1</sup>	elevation head			
P-100.2	5190.06 <sup>1</sup>	5190.06 <sup>1</sup>	elevation head			
P-100.3	5183.23 <sup>1</sup>	5183.23 <sup>1</sup>	elevation head			
P-101.1	5185.93 <sup>1</sup>	5185.93 <sup>1</sup>	elevation head			
P-101.2	5183.13	5184.20	elevation head			
P-101.3	5171.25	5173.18	elevation head			
P-102.1	5188.85 <sup>1</sup>	5188.85 <sup>1</sup>	elevation head			
P-102.2	5174.60 <sup>1</sup>	5174.60 <sup>1</sup>	elevation head			
P-102.3	5167.69	5168.90	elevation head			
P-103.1	5185.91 <sup>1</sup>	5185.91 <sup>1</sup>	elevation head			
P-103.2	5170.91 <sup>1</sup>	5170.91 <sup>1</sup>	elevation head			
P-103.3	5160.24 <sup>1</sup>	5160.91	elevation head			
P-104.1	5198.72 <sup>1</sup>	5198.72 <sup>1</sup>	elevation head			
P-104.2	5185.47 <sup>1</sup>	5185.47 <sup>1</sup>	elevation head			
P-104.3	5178.47 <sup>1</sup>	5178.47 <sup>1</sup>	elevation head			
P-105.1	5184.82 <sup>1</sup>	5184.88	elevation head			
P-105.2	5174.16 <sup>1</sup>	5174.16 <sup>1</sup>	elevation head			
P-105.3	5162.16 <sup>1</sup>	5162.71	elevation head			
P-106.1	5186.09 <sup>1</sup>	5186.09 <sup>1</sup>	elevation head			
P-106.2	5165.51 <sup>1</sup>	5165.51 <sup>1</sup>	elevation head			
P-106.3	5160.46	5160.91	elevation head			
P-107.1	5197.27 <sup>1</sup>	5197.42	elevation head			
P-107.3	5173.44 <sup>1</sup>	5173.44 <sup>1</sup>	elevation head			
P-108.1	5184.26 <sup>1</sup>	5184.26 <sup>1</sup>	elevation head			
P-108.2	5173.59 <sup>1</sup>	5173.59 <sup>1</sup>	elevation head			
P-108.3	5172.32	5173.86	elevation head			
P-109.1	5188.76 <sup>1</sup>	5188.76 <sup>1</sup>	elevation head			
P-109.2	5172.51 <sup>1</sup>	5172.51 <sup>1</sup>	elevation head			
P-109.3	5164.93 <sup>1</sup>	5165.07	elevation head			
P-110.1	5184.28 <sup>1</sup>	5184.61	elevation head			
P-110.2	5171.86 <sup>1</sup>	5171.86 <sup>1</sup>	elevation head			
P-110.3	5163.44 <sup>1</sup>	5163.44 <sup>1</sup>	elevation head			
P-111.1	5187.29 <sup>1</sup>	5187.29 <sup>1</sup>	elevation head			
P-111.2	5172.33 <sup>1</sup>	5172.33 <sup>1</sup>	elevation head			
P-111.3	5160.34	5160.56	elevation head			
<sup>1</sup> Porewater pressure measurements are negative (draining condition)						

Instrument Name	Minimum	Maximum	Unit					
	Survey Monuments	(10/1/17 to 3/8/18)						
SM7	5215.911	5215.957	EL (ft)					
SM9	5217.089	5217.151	EL (ft)					
	Settlement Rods (1	0/1/17 to 3/8/18)						
SR-7	5250.791	5250.869	EL (ft)					
SR-8	5256.226	5256.313	EL (ft)					
SR-9	5248.651	5248.691	EL (ft)					
SR-10	5248.879	5248.948	EL (ft)					
SR-100	5222.279	5222.321	EL (ft)					
SR-101	5205.501	5205.538	EL (ft)					
SR-102	5205.314	5205.411	EL (ft)					
SR-104	5219.336	5219.379	EL (ft)					
SR-105	5205.008	5205.079	EL (ft)					
SR-106	5205.321	5205.391	EL (ft)					
SR-109	5206.549	5206.620	EL (ft)					
SR-110	5205.831	5205.921	EL (ft)					
	Inclinometers (10/	1/17 to 9/30/18)						
I-1	0	0.1380	in					
I-2	0	0.1422	in					
I-103	0	0.1668	in					
I-107	0	0.1206	in					
I-111	0	0.0672	in					
Oper	Open Standpipe Piezometers (10/1/17 to 9/30/18)							
P-23	5157.00	5157.09	EL (ft)					
P-24	Dry	Dry	EL (ft)					
P-25	Dry	Dry	EL (ft)					

The data for the piezometers over the current review period indicate no significant elevation changes or trends related to the performance of the dam.

The data for the survey monuments and settlement rods indicate no significant elevation changes or negative trends related to the performance of the dam. No survey data is available after March 8, 2018.

The data for the inclinometers over the current review period indicate no significant elevation changes or trends related to the performance of the dam.

# 5.1.3 CCR and Water Elevations

The approximate minimum, maximum, and present depth and elevation of the impounded water and CCR since the previous annual inspection is presented in the following table:

Water	Depth of Water (ft)	Water Elevation (ft)	Measurement Location
Minimum	N/A	N/A	N/A
Maximum	N/A	N/A	N/A
Present (this inspection)	4.7	5274.2	Southwest Corner (STA 36+00)
CCR	Depth of CCR (ft)	CCR Elevation (ft)	Measurement Location
Minimum	12.47	5286.47	Emergency Ladder on the north end of the LAI (STA 87+04)
Maximum	70	5275	Emergency Ladder on the West Embankment near the Drop Inlet Structure
Present (this inspection)	70	5275	Emergency Ladder on the West Embankment near the Drop Inlet Structure

APS does not normally record the water level in the LAI. The present depth of water (4.7 feet) assumes ash up to EL 5269.5 feet in the Southwest Corner of the impoundment, a value recorded in 2014 prior to the ash being submerged at STA 36+00.

#### 5.1.4 Storage Capacity

The estimated remaining maximum storage capacity of the LAI at the time of the inspection was 633.84 acre-feet (ac-ft).

#### 5.1.5 Approximate Impounded Volume at Time of Inspection

The approximate volume of impounded CCR in the LAI at the time of the inspection was 5,352.16 ac-ft.

#### 5.1.6 Structural Weakness or Operational Change/Disruption

No conditions associated with structural weakness were identified during the field inspection.

Holes appeared to have been cut in the geomembrane liner along the western portion of the South Embankment in the area where water was trapped underneath the liner during the 2017 inspection. Three of the holes appeared to be allowing the upstream clay blanket to erode into the impoundment. It was not clear during the inspection how long the clay had been eroding or how much volume had been lost. A fourth hole was leaking water during the inspection and it was not clear if any clay had previously eroded or if clay would erode in the future. In addition, a depression and two bulges were observed along the upstream slope in the same area. These features, combined with the increased water flowing to the LAI from the Plant, have the potential to disrupt the normal operation of the LAI; however, the LAI was designed to be stable without the presence of the geosynthetic HDPE liner.

There are no significant changes to the structural integrity or operation of the dam since the 2017 inspection.

# 5.2 LINED DECANT WATER POND

# 5.2.1 Geometry Changes Since Last Inspection

There have not been any significant changes to the geometry of the unit since the last inspection in 2017.

# 5.2.2 Instrumentation

The locations of geotechnical and other related instrumentation in the vicinity of the LDWP are shown on Figure 7 – Lined Decant Water Pond (LDWP) Instrumentation Map.

The minimum and maximum recorded readings for each instrument over the October 1, 2017 – September 30, 2018 (current) review period are reported in the following table:

Instrument Name	Minimum	Maximum	Unit						
Survey Monuments (10/1/17 to 3/8/18)									
SM7	5215.911	5215.957	EL (ft)						
SM9	5217.089	5217.151	EL (ft)						
Oper	Open Standpipe Piezometers (10/1/17 to 9/30/18)								
P-18	Dry	Dry	EL (ft)						
P-19	Dry	Dry	EL (ft)						
P-20	Dry	Dry	EL (ft)						
P-21	Dry	Dry	EL (ft)						
P-22	Dry	Dry	EL (ft)						
P-23	5157.00	5157.09	EL (ft)						
P-24	Dry	Dry	EL (ft)						
P-25	Dry	Dry	EL (ft)						

The data for the survey monuments over the current review period indicate no significant elevation changes or trends related to the performance of the dam.

The data for the piezometers over the current review period indicate no significant elevation changes or trends related to the performance of the dam.

#### 5.2.3 CCR and Water Elevations

The approximate minimum, maximum, and present depth and elevation of the impounded water and CCR since the previous annual inspection is presented in the following table:

Water	Depth of Water (ft)	Water Elevation (ft)	<b>Measurement Location</b>
Minimum	1.0	5206.0	Staff gauge near the East Embankment
Maximum	4.6	5209.6	Staff gauge near the East Embankment
Present (this inspection)	1.8	5206.8	Staff gauge near the East Embankment
CCR	Depth of CCR (ft)	CCR Elevation (ft)	<b>Measurement Location</b>
Minimum	Not Applicable	Not Applicable	Not Applicable
Maximum	Not Applicable	Not Applicable	Not Applicable
Present (this inspection)	Not Applicable	Not Applicable	Not Applicable

The LDWP does not impound a significant quantity of solids. It is used to impound CCR-transport water decanted from the LAI.

#### 5.2.4 Storage Capacity

The estimated maximum remaining storage capacity of the LDWP at the time of the inspection was approximately 362 ac-ft.

# 5.2.5 Approximate Impounded Volume at Time of Inspection

The approximate volume of impounded water in the LDWP at the time of the inspection was 155 ac-ft.

#### 5.2.6 Structural Weakness or Operational Change/Disruption

No conditions associated with structural weakness were identified during the field inspection.

No conditions that are or could be disruptive to the operation and safety of the CCR unit and appurtenant structures were identified during the field inspection.

There are no significant changes to the structural integrity or operation of the dam since the 2017 inspection.

# 5.3 COMBINED WASTE TREATMENT POND

## 5.3.1 Geometry Changes Since Last Inspection

There have not been any significant changes to the geometry of the unit since the last inspection in 2017.

# 5.3.2 Instrumentation

There are no instruments associated with the CWTP.

# 5.3.3 CCR and Water Elevations

The approximate minimum, maximum, and present depth and elevation of the impounded water and CCR since the previous annual inspection is presented in the following table:

Water	Depth of Water (ft)	Water Elevation (ft)	Measurement Location
Minimum	N/A	N/A	APS does not regularly record the
Maximum	N/A	N/A	water elevation.
Present (this inspection)	~10	5329 (NGVD29)	Spillway Crest
CCR	Depth of CCR (ft)	CCR Elevation (ft)	<b>Measurement Location</b>
Minimum	N/A	N/A	N/A
Maximum	N/A	N/A	N/A
Present (this inspection)	7.68	5319 (NGVD29)	Assumed from 2016 bathymetry*

\*The majority of the solids are caught in the decant cells on the west side of the CWTP.

CCR solids in the CWTP reservoir are typically submerged and periodically dredged; however, the typical CCR elevation is assumed to be approximately EL 5322 feet (NAVD88; approximate EL 5319 feet NGVD29) based on historic bathymetry.

APS does not regularly record or track the water elevation in the CWTP. Water in the CWTP normally overflows a weir on the east side of the reservoir and flows into Morgan Lake. The elevation of the water as it flows over the weir wall is generally constant at EL 5329 feet.

# 5.3.4 Storage Capacity

The estimated maximum remaining storage capacity of the CWTP reservoir at the time of the inspection was 27 ac-ft based on historic topography and bathymetry.

# 5.3.5 Approximate Impounded Volume at Time of Inspection

The approximate volume of impounded water and solids in the CWTP reservoir at the time of the inspection was 137 ac-ft.

#### 5.3.6 Structural Weakness or Operational Change/Disruption

The inspection identified longitudinal cracks forming along the downstream slope of the eastern CWTP embankment above the water line. The area should be monitored and the cracks should be repaired to prevent a disruption to the normal operation of the CCR unit if they are observed to expand.

There are no significant changes to the structural integrity or operation of the dam since the 2017 inspection.

#### 5.4 UPPER RETENTION SUMP

#### 5.4.1 Geometry Changes Since Last Inspection

APS is in the process of replacing the existing Upper Retention Sump with a concrete tank and will remove the existing Upper Retention Sump from service when construction is complete. To make room for the construction activities, the existing Upper Retention Sump has been significantly reduced in size since the previous annual inspection in 2017 (Appendix D). The southern portion of the CCR unit's footprint, as delineated by a block wall faced with geomembrane (to prevent leaks), is the only remaining section being utilized. The volume available to store CCR solids and CCR- transport water is approximately 0.643 acre-feet.

#### 5.4.2 Instrumentation

There are no instruments associated with the Upper Retention Sump.

## 5.4.3 CCR and Water Elevations

The current CCR elevation is approximately 5339.25 feet. The current water elevation is approximately 5339.25 feet. The current CCR and water elevations represent approximately 3 inches of impounded depth.

## 5.4.4 Storage Capacity

The estimated maximum remaining storage capacity of the Upper Retention Sump at the time of the inspection was approximately 0.643 ac-ft.

## 5.4.5 Approximate Impounded Volume at Time of Inspection

The approximate volume of impounded water and CCR solids in the Upper Retention Sump at the time of the inspection was less than 0.01 ac-ft.

## 5.4.6 Structural Weakness or Operational Change/Disruption

No conditions associated with structural weakness were identified during the field inspection.

No conditions that are or could be disruptive to the operation and safety of the CCR unit and appurtenant structures were identified during the field inspection.

To maintain a safe working area for construction activities, the Upper Retention Sump has been significantly dewatered since the previous annual inspection in 2017 (Appendix D). A negligible volume of CCR solids and CCR-transport water was impounded at the time of the inspection.

#### 5.5 DRY FLY ASH DISPOSAL AREA

#### 5.5.1 Geometry Changes Since Last Inspection

Site 3 continued to receive ash loading after the 2017 inspection. Site 3 is divided into approximately three sequential sections from the east to the west. APS places ash in these sections from east to west to maintain a grade that will allow stormwater to drain off the west side of Site 3 to the lined leachate cell collection ponds.

#### 5.5.2 Instrumentation

There are no instruments associated with the DFADA.

#### 5.5.3 CCR Volume

The approximate volume of CCR in the DFADA at the time of the inspection was estimated to be 4,642 ac-ft based on the July 2018 survey performed by the ash placement contractor (FHI).

#### 5.5.4 Structural Weakness or Operational Change/Disruption

No conditions associated with structural weakness were identified during the field inspection.

No conditions that are or could be disruptive to the operation and safety of the CCR unit and appurtenant structures were identified during the field inspection.

There are no significant changes to the structural integrity or operation of the landfill since the 2017 inspection.

## 6.0 OPERATION AND MAINTENANCE RECOMMENDATIONS

The following items were noted during inspections as requiring attention.

## 6.1 LINED ASH IMPOUNDMENT

Observed Condition		Action Item
1)	Water and clay were observed to be leaking out of four holes cut in the geomembrane liner along western portion of the South Embankment.	Repair the holes, investigate the approximate loss of clay, and repair the portion of clay that was lost. Determine why and how the liner was cut. Implement rules to prevent future damage to the liner and upstream clay blanket.
2)	There are two bulges and a depression along the upstream slope in the Southwest Corner of the LAI.	The bulges and depression should be investigated and repaired. Bulges appear to be clay liner material eroded and deposited from tears in the liner repaired earlier (2017). Investigate depression and repair with clay material as needed.
3)	There is a single-walled HDPE pipe along the West Embankment crest being used to pump water from the Southwest Corner to the Drop Inlet Structure.	The pipe should be moved inside the impoundment.
4)	The downstream slopes of the West Embankment and the Northwest Embankment have minor erosion rills.	Continue ongoing repair program for repairing rills if the erosion depth exceeds 1 foot.
5)	There are small tears and holes in the liner on the crest of the East Embankment.	Repair the tears.

#### 6.2 LINED DECANT WATER POND

Observed Condition		Action Item
1)	Two sloughs were observed on the	Repair the areas and monitor the slope.
	lowermost bench of the West	
	Embankment.	
2)	The liner in the anchor trench in the	Investigate the cause of the damage and repair
	central portion of the West Embankment	the liner as necessary.
	appeared to be pulling out of the trench.	
3)	Minor erosion rilling was observed on the	Continue ongoing repair program for
	North and West downstream slopes of the	repairing rills if the erosion depth exceeds 1
	LDWP at the time of the inspection.	foot.
4)	There are small holes and tears in the liner	Repair the tears and holes.
	along the North and East Embankments.	

## 6.3 COMBINED WASTE TREATMENT POND

Observed Condition	Action Item
<ol> <li>Vegetation removal along the upstream and downstream slopes should be performed in accordance with the NMOSE vegetation maintenance guidelines "Vegetation Management on Dams" (2011) reference.</li> </ol>	This is an ongoing maintenance requirement.
<ol> <li>Several instances of minor erosion were observed on the downstream slope above the riprap.</li> </ol>	Continue ongoing repair program for repairing erosion if the erosion depth exceeds 1 foot.
3) Longitudinal cracks along the downstream slope above the riprap.	Monitor the area and repair the slope if the cracks expand, deepen, or result in a slough/slide.
<ul><li>4) Erosion along the upstream slope resulting in an irregular face.</li></ul>	Continue to monitor the area repair the area if required to bring it to the design slope (2H:1V).
5) Shallow erosion holes in the crest.	Monitor the erosion holes and repair them if they exceed 1 foot deep or if additional erosion holes are observed.
6) Continue to monitor the embankment for animal burrows.	This is an ongoing maintenance requirement. Repair animal burrows as needed.

## 6.4 UPPER RETENTION SUMP

Observed Condition	Action Item
No deficient conditions were observed during	N/A
the inspection.	

## 6.5 DRY FLY ASH DISPOSAL AREA

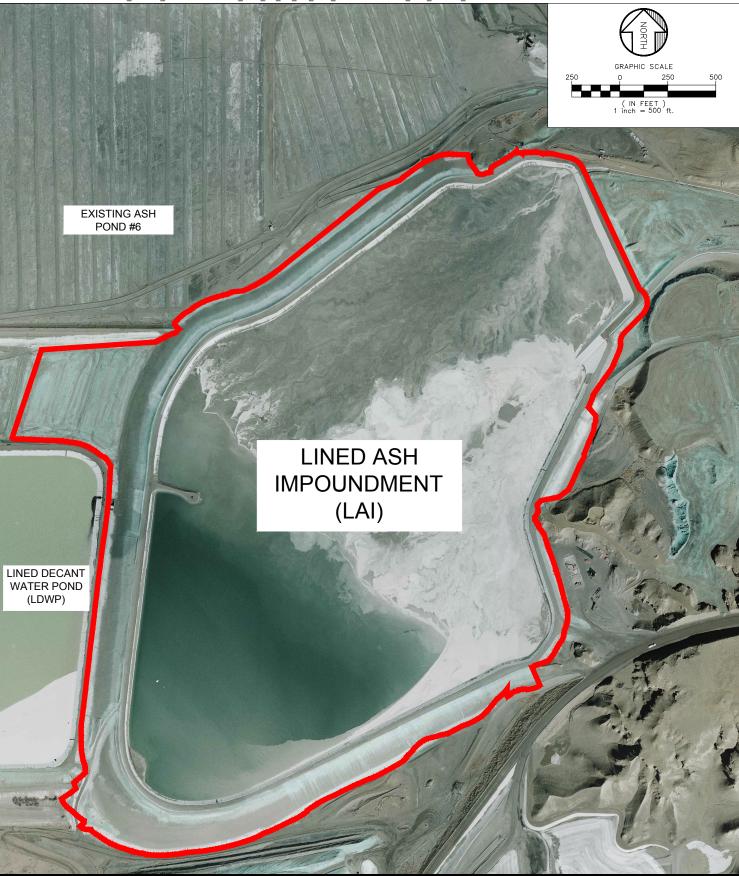
Observed Condition	Action Item
<ol> <li>There is erosion at the inlet and outlet of the Stormwater Diversion Channel.</li> </ol>	With future expansion of the DFADA, perform an engineering re-evaluation to understand whether the run off pattern has changed or whether a different erosion control method should be applied. Monitor erosion and repair as required. Alternately, place additional sandstone riprap in the eroded area.
2) Several plants are growing through the Pyramat geosynthetic along the western toe of Cell 1.	Monitor the plant growth and remove the vegetation if it is determined to be damaging the primary geomembrane liner.
<ol> <li>Vacuum truck operators were allowing ash to be blown across the site while it was being unloaded.</li> </ol>	Monitor contractor activities and enforce dust control plan.

## 7.0 REFERENCES

- Arizona Public Service Corporation and AECOM. 2016. Four Corners Power Plant Lined Ash Impoundment, Lined Decant Water Pond, Combined Waste Treatment Pond, Upper Retention Sump, and Dry Fly Ash Disposal Area – Annual CCR Impoundment and Landfill Inspection Report – 2015. January.
- Arizona Public Service Corporation. 2017. Four Corners Power Plant Lined Ash Impoundment, Lined Decant Water Pond, Combined Waste Treatment Pond, Upper Retention Sump, and Dry Fly Ash Disposal Area – Annual CCR Impoundment and Landfill Inspection Report – 2016. January.
- Arizona Public Service Corporation. 2018. Four Corners Power Plant Lined Ash Impoundment, Lined Decant Water Pond, Combined Waste Treatment Pond, Upper Retention Sump, and Dry Fly Ash Disposal Area – Annual CCR Impoundment and Landfill Inspection Report – 2017. January.
- Federal Emergency Management Agency. 2005. Technical Manual for Dam Owners, Impacts of Plants on Earthen Dams, FEMA Manual 534. September.
- New Mexico Office of the State Engineer (NMOSE). Dam Safety Bureau. 2011. Vegetation Management on Dams. 3 pgs. August 15.
- National Oceanic and Atmospheric Administration (NOAA), Web. 2018. "Climate Data Online Search for Farmington, New Mexico." < https://www.ncdc.noaa.gov/cdo-web/search>. 29 November.
- United States Environmental Protection Agency (EPA), 2015. 40 CFR Parts 257 and 261 Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule. Federal Register Vol. 80, No. 74. April 17.
- URS Corporation, 2012. Engineering Design Report Lined Ash Impoundment 5280 Lift Four Corners Power Plant – San Juan County, New Mexico – NMOSE File No. D-634. Prepared for Arizona Public Service. March.

## **FIGURES**





LINED ASH IMPOUNDMENT (LAI)





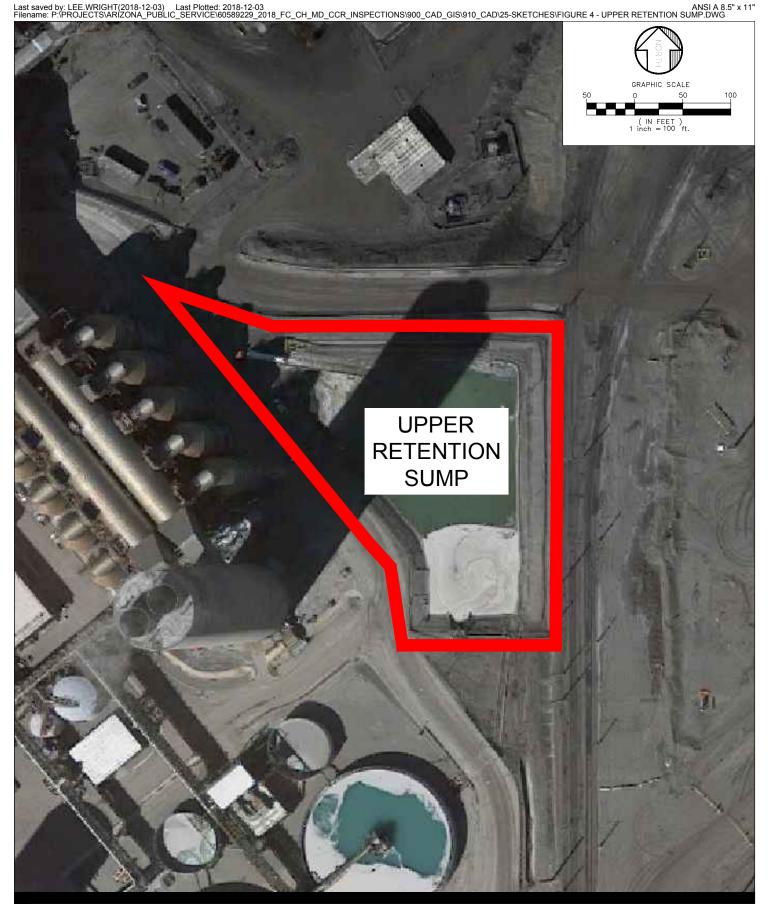
LINED DECANT WATER POND (LDWP)





COMBINED WASTE TREATMENT POND (CWTP)





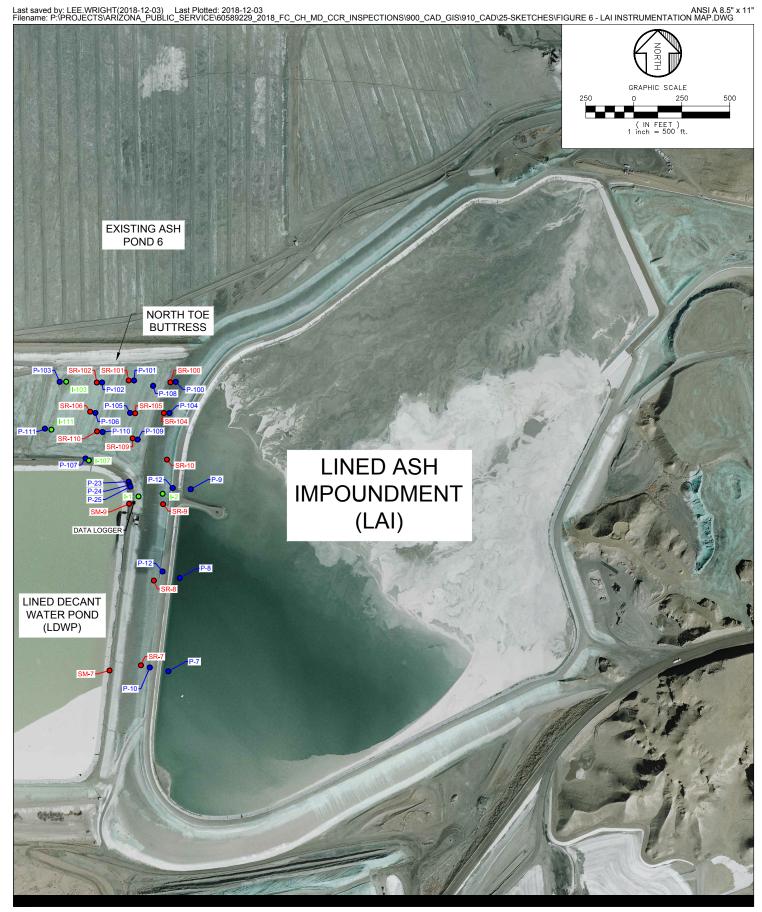
UPPER RETENTION SUMP





DRY FLY ASH DISPOSAL AREA (DFADA)





LINED ASH IMPOUNDMENT (LAI) INSTRUMENTATION MAP



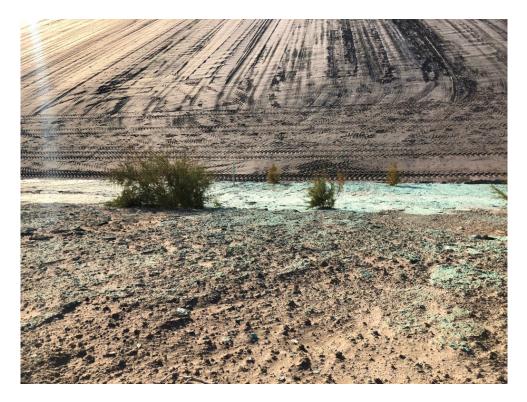


LINED DECANT WATER POND (LDWP) INSTRUMENTATION MAP



## **APPENDIX A**

# LINED ASH IMPOUNDMENT (LAI) PHOTO LOG



Woody vegetation growing on the downstream slope of the South Embankment.



**20181025 – IMG\_1204** The crest of the South Embankment, facing west.



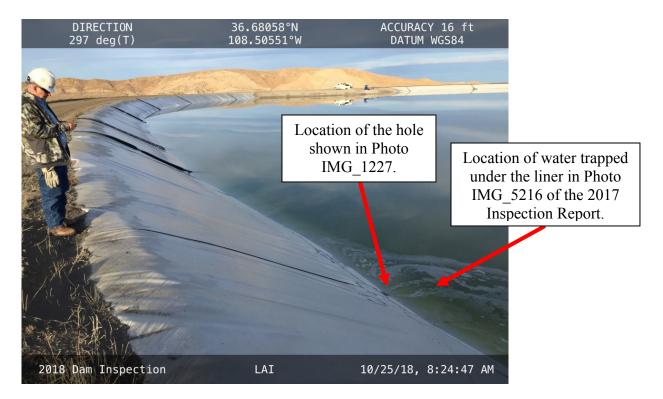
The downstream slope of the South Embankment, facing west.



**20181025 – IMG\_1206** The upstream slope of the South Embankment, facing west.



Water flowing back into the LAI through a hole cut in the geomembrane liner along the South Embankment.



## 20181025 – IMG\_1229

The upstream slope in the Southwest Corner, facing west.

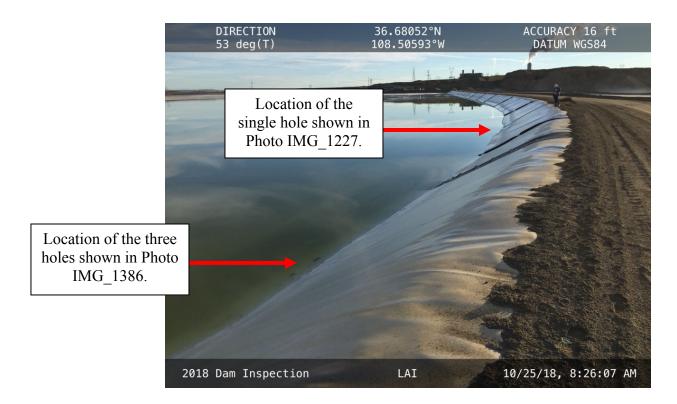


Depression along the upstream slope of the South Embankment between holes cut in the liner.



## 20181025 - IMG\_1386

Clay eroding out of three holes cut in the liner along the upstream slope of the South Embankment.



The upstream slope along the South Embankment with holes in the liner annotated, facing east.



## 20181025 - IMG\_1244

Bulges in the geomembrane liner in the Southwest Corner of the LAI.



The portable pump APS uses to pump water out of the LAI and into the Drop Inlet Structure.



## 20181025 - IMG\_1254

The upstream slope of the West Embankment, facing north from the South Embankment.



The crest of the West Embankment, facing north from the Southwest Corner.

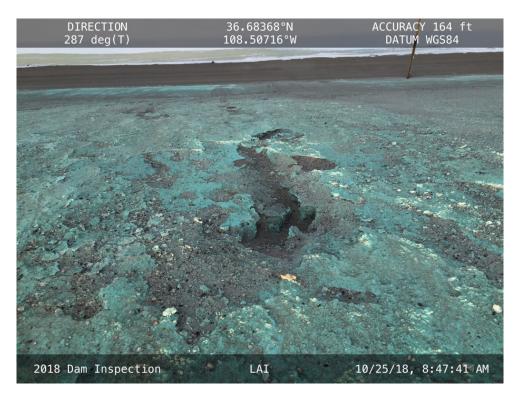


## 20181025 - IMG\_1256

The HDPE pipe that conveys water from the pump in the Southwest Corner to the Drop Inlet Structure.



The downstream slope and crest of the West Embankment, facing north.



**20181025 – IMG\_1269** Minor erosion on the downstream slope of the West Embankment.



Water being pumped from the Southwest Corner of the LAI into the Drop Inlet Structure.



## 20181025 - IMG\_1293

The upstream slope of the West Embankment, facing north from the emergency ladder next to the Drop Inlet Structure.



The North Toe Buttress, facing northwest from the crest of the West Embankment.



#### 20181025 - IMG 1305

The crest of the West Embankment, facing north from the Northwest Corner.



The crest of the West Embankment, facing south from the Northwest Corner.



## 20181025 - IMG\_1017

Minor erosion rills along the downstream slope of the West Embankment near the NTB.



The upstream slope of the Northwest Embankment, facing northeast from the Northwest Corner.



## 20181025 - IMG\_1313

The downstream slope of the Northwest Embankment, facing northeast.



The crest of the Northwest Embankment, facing northeast.



**20181025 – IMG\_1333** The crest of the Northwest Embankment, facing northeast.



The downstream slope of the Northwest Embankment, facing west.



#### 20181025 - IMG 1338

Shallow erosion rill in the groin of the Northwest Embankment along the north end of the LAI.



The upstream slope in the northernmost portion of the LAI, facing west.



#### 20181025 - IMG 1356

The crest along the northern end of the East Embankment, facing southeast.



The crest and upstream slope of the East Embankment, facing southeast.

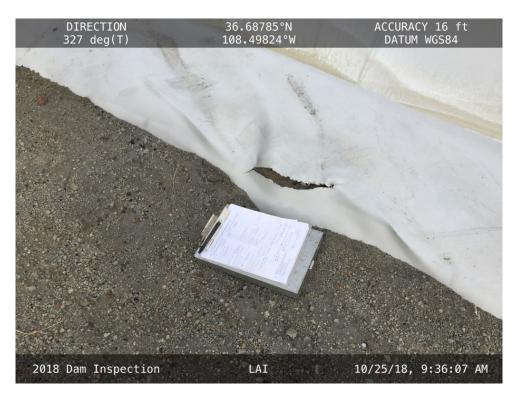


## 20181025 - IMG\_1358

A small scratch and indentation in the liner along the East Embankment.



FGD sludge being deposited into the LAI from the V-ditch at the East Embankment.



**20181025 – IMG\_1373** A tear in the liner near the V-ditch at the East Embankment.



A small hole in the liner near the V-ditch at the East Embankment.



#### 20181025 - IMG 1378

The upstream slope of the East Embankment near the abandoned V-ditch, facing southwest.



The downstream slope of the East Embankment, facing south.



#### 20181025 - IMG\_1388

The downstream slope of the West Embankment, facing north along the toe.



The downstream toe of the West Embankment, facing north.



**20181025 – IMG\_1415** The South Embankment toe drain in a dry condition.

## **APPENDIX B**

# LINED DECANT WATER POND (LDWP) PHOTO LOG



The South Embankment of the LDWP, facing west from the crest of the LAI.



#### 20181025 - IMG\_1413

The staff gauge and water elevation markings on the east side of the LDWP.



A shallow surface slough on the lowermost bench of the West Embankment.



#### 20181025 - IMG\_1438

A second shallow surface slough on the lowermost bench of the West Embankment.



The toe and downstream slope of the South Embankment, facing east.



#### 20181025 - IMG\_1442

The South Embankment of the LDWP along the upper berm, facing west.



The Deadpool Sump control panels (no longer in use).



**20181025 – IMG\_1446** The upstream slope of the South Embankment, facing west.



**20181025 – IMG\_1447** The crest of the South Embankment, facing west.



**20181025 – IMG\_1448** The downstream slope of the South Embankment, facing west.



The upstream slope of the East Embankment, facing northeast from the South Embankment.



#### 20181025 - IMG\_1459

The upstream slope of the West Embankment, facing northwest from the South Embankment.



**20181025 – IMG\_1463** The Interstitial Evacuation Pump control panel.



**20181025** – **IMG\_1471** The HDPE pipes associated with the Interstitial Evacuation Pump.



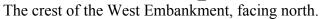
The upstream slope of the West Embankment, facing north from the South Embankment.



#### 20181025 - IMG\_1480

The upstream slope of the South Embankment, facing east from the West Embankment.







#### **20181025 – IMG\_1489** The downstream slope of the West Embankment, facing north.



The discharge pipe from the Pond 3 Pump House along the West Embankment.



**20181025 – IMG\_1506** The downstream slope of the West Embankment, facing north.



The liner pulling out of the anchor trench in the northern portion of the West Embankment.



#### 20181025 - IMG\_1515

The northwest corner of the LDWP, facing north from the West Embankment.



A shallow dent in the liner in the northwest corner of the LDWP.



**20181025 – IMG\_1526** The crest of the North Embankment, facing east.



20181025 – IMG\_1528

The downstream slope of the North Embankment, facing east.



#### 20181025 - IMG\_1529

A hole in the liner along the North Embankment already marked with a pin flag.



Small tears in the liner along the North Embankment already marked with a pin flag (these were also observed during the 2017 inspection).



#### 20181025 - IMG\_1531

The northeast corner of the LDWP, facing east from the North Embankment.



The downstream slope of the North Embankment, facing west.



**20181025 – IMG\_1540** The upstream slope of the East Embankment, facing south.



The surface monuments for piezometers P-23, P-24, and P-25.



#### 20181025 - IMG\_1547

The 8-inch and 16-inch HDPE outlet pipes conveying decant water from the LAI.



The LDWP pump station in the northeast corner of the perimeter embankment.



#### 20181025 - IMG\_1556

The LDWP pump station in the northeast corner of the perimeter embankment.



The liner pulling out of the anchor trench in the East Embankment.



**20181025 – IMG\_1566** The crest of the East Embankment, facing south.



A tear in the liner along the East Embankment (also observed during the 2017 inspection).



#### $20181025 - IMG\_1572$

Shallow dents in the liner along the upstream slope of the East Embankment.



The upstream slope of the East and South Embankments, facing south.



**20181025 – IMG\_1580** The upstream slope of the East Embankment, facing north.

## **APPENDIX C**

# COMBINED WASTE TREATMENT POND (CWTP) PHOTO LOG



**20181024 – IMG\_0888** The outfall from the CWTP to the discharge canal.



The crest and upstream slope of the CWTP, facing east from the West Abutment.



The crest of the CWTP, facing east from the West Abutment.



#### 20181024 - IMG\_0909

The downstream slope of the CWTP, facing east from the West Abutment.



A shallow erosion rill on the downstream slope of the CWTP embankment.



# **20181024 – IMG\_0914**

Vegetation on the downstream slope  $\overline{of}$  the CWTP embankment.



Vegetation and riprap along the waterline of the downstream slope.



**20181024 – IMG\_0920** The crest of the CWTP embankment, facing east.



Woody vegetation to be removed from the downstream slope.



**20181024 – IMG\_0923** The downstream slope of the CWTP embankment, facing east.



**20181024 – IMG\_0927** Erosion at the waterline along the downstream slope.



**20181024 – IMG\_0931** Erosion holes along the downstream shoulder of the crest.



Longitudinal cracks on the downstream slope of the CWTP embankment.



#### 20181024 - IMG\_0947

The crest of the CWTP embankment, facing northwest from the South Abutment.



The upstream slope and reservoir, facing northwest from the South Abutment.



#### 20181024 - IMG\_0952

Woody vegetation on the upstream slope near the South Abutment, facing north.

8



**20181024 – IMG\_0954** The upstream slope of the CWTP, facing west.



**20181024 – IMG\_0959** The crest of the CWTP embankment, facing west.



The upstream slope along the northern portion of the embankment, facing west.



**20181024 – IMG\_0964** The crest of the CWTP embankment, facing east.



**20181024 – IMG\_0969** The forebay pond on the west side of the CWTP.

## **APPENDIX D**

# **UPPER RETENTION SUMP PHOTO LOG**



20181024 - IMG\_0842

Construction of the Upper Retention Sump (URS) Tank in the URS basin, facing north.



**20181024 – IMG\_0847** The south end of the Upper Retention Sump, facing southeast.

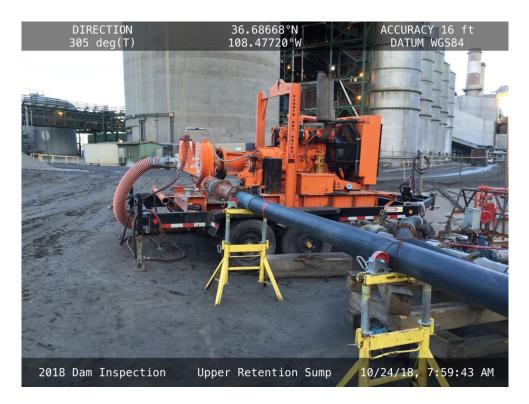


The south end of the Upper Retention Sump, facing the east cofferdam area.



### 20181024 - IMG\_0866A

A temporary wall delineating the northern boundary of the Upper Retention Sump, facing north.



Temporary pumping equipment on the south side of the Upper Retention Sump.



### 20181024 - IMG\_0861

Inlet pipes rerouted to the remaining footprint of the Upper Retention Sump, facing west.



Construction of the Upper Retention Sump Tank adjacent to the Upper Retention Sump.



### 20181024 - IMG\_0864

The upstream slope along the east side of the Upper Retention Sump footprint, facing north.



### 20181024 - IMG\_0866B

The south side of the Upper Retention Sump, facing west.



#### 20181024 - IMG\_0867

The south side of the Upper Retention Sump and Upper Retention Sump Tank, facing west.



**20181024 – IMG\_0869** Construction of the Upper Retention Sump Tank, facing west.



**20181024 – IMG\_0870** The upstream slope along the east side of the Upper Retention Sump footprint, facing south.



Construction of the Upper Retention Sump Tank, facing northwest.



## 20181024 – IMG\_0886

The north side of the Upper Retention Sump footprint, facing west.



Construction of the Upper Retention Tank Sump in the URS footprint, facing south.



### 20181024 - IMG\_0890

Construction of the Upper Retention Sump Tank in the URS footprint, facing south.



### **20181024 – IMG\_0898** The north side of the Upper Retention Sump footprint, facing east.

### **APPENDIX E**

# DRY FLY ASH DISPOSAL AREA (DFADA) PHOTO LOG



**20181024 – IMG\_0933** Area of erosion repair along the western toe of Cell 3, facing north.



**20181024 – IMG\_0937** Area of additional erosion along the western toe of Cell 3 north of IMG\_0933, facing north.



The east side of DFADA Cell 2, looking southwest from the ash haul road.



### 20181024 - IMG\_1130

Dust generated by a vacuum truck along the southeast side of DFADA Cell 2.



The south slope of DFADA Cell 2, facing west along the toe.



**20181024 – IMG\_1134** The south slope of DFADA Cell 2, facing east along the toe.



The south slope of DFADA Cell 1, facing west along the toe.



### 20181024 - IMG\_1136

Woody vegetation growing through the Pyramat in the southwest corner of Cell 1.



The leachate collection pond for DFADA Cell 2, facing north from the south berm.



**20181024 – IMG\_1140** The west side of DFADA Cell 1, facing north.



The leachate collection pond for DFADA Cell 1, facing northeast from the west side.



**20181024 – IMG\_1150** A repair in the DFADA Cell 1 leachate collection pond liner.



Vegetation growing in the drainage ditch and overflow channel of the leachate collection pond.



### 20181024 - IMG\_1157

Woody vegetation growing through the Pyramat on the western toe of DFADA Cell 1.



DFADA Cell 3, facing east from the South Embankment of the LAI.



### 20181024 - IMG\_1202

The easternmost portion of DFADA Cell 3, facing east from the South Embankment of the LAI.



DFADA Cell 2 (background) and the central portion of Cell 3 (foreground), facing south.



**20181025 – IMG\_1224** DFADA Cell 1 and the western portion of Cell 3, facing southwest.



The leachate collection ponds and the western portions of DFADA Cells 1 and 3, facing south.



### 20181025 - IMG\_1417

The Stormwater Diversion Channel around the eastern edge of DFADA Cell 2, facing east.



Erosion at the Stormwater Diversion Channel outlet, facing west.



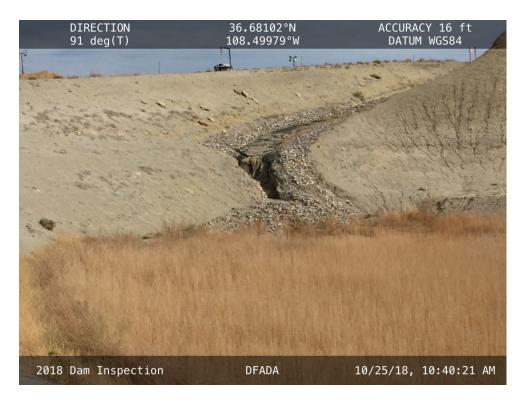
**20181025 – IMG\_1423** Sediment in the Stormwater Diversion Channel near the outlet.



**20181025 – IMG\_1425** The south slope of DFADA Cell 1, facing northwest.



**20181025 – IMG\_1426** The south slope of DFADA Cells 1 and 2, facing north.



Inlet to the Stormwater Diversion Channel, facing east from the ash haul road.