Arizona Public Service
Cholla Power Plant

Fly Ash Pond

Location Restrictions
Demonstration Report

Prepared for:
Arizona Public Service

AECOM Job No. 60587726
October 8, 2018
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Certification Statement

Certification Statement for Location Restrictions:

- 40 CFR § 257.60 – Placement above the uppermost aquifer
- 40 CFR § 257.61 – Wetlands
- 40 CFR § 257.62 – Fault areas
- 40 CFR § 257.63 – Seismic impact zones
- 40 CFR § 257.64 – Unstable Areas

CCR Unit: Arizona Public Service Company; Cholla Power Plant; Fly Ash Pond

I, Alexander Gourlay, being a Registered Professional Engineer in good standing in the State of Arizona, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR unit, that the demonstration regarding the location of the CCR unit in the wetlands, the demonstration regarding the location of the CCR unit within 60 meters (200 feet) of the outermost damage zone of a fault that has had a displacement in Holocene time, the demonstration regarding the location of the CCR unit in a seismic impact zone, and the demonstration that the location of the CCR unit is not in an unstable area, as included in the Location Restrictions Demonstration Report dated October 8, 2018 meets the requirements of 40 CFR § 257.61(a), § 257.62(a), § 257.63(a), and § 257.64(a). I certify, for the above-referenced CCR unit, that the demonstration regarding the location of the CCR unit less than 1.52 meters (5 feet) above the upper limit of the uppermost aquifer does not meet the requirements of 40 CFR § 257.60(a).

Alexander W. Gourlay, P.E.

Printed Name

October 8, 2018

Date
1 Introduction

Arizona Public Service Company (APS) contracted AECOM to assist in the location restriction demonstrations of the existing coal combustion residual (CCR) surface impoundments at the Cholla Power Plant (Cholla, the Plant) near Joseph City, in Navajo County, Arizona. Figure 1-1 shows the location of the CCR Impoundments at Cholla. This Demonstration Report documents location-specific conditions relevant to the Fly Ash Pond.

1.1 Report Purpose and Description

The purpose of this report is to document the location restriction demonstration for the Fly Ash Pond. The Fly Ash Pond is an existing CCR surface impoundment owned and operated by APS. In 2015, the United States Environmental Protection Agency (EPA) finalized a rule (Rule) regulating CCRs under subtitle D of the Resource Conservation and Recovery Act (RCRA). As part of this Rule, owners and operators of existing surface CCR impoundments must obtain a certification from a qualified professional engineer stating that the demonstrations for the CCR unit meet the requirements relative to the uppermost aquifer, wetlands, fault areas, seismic impact zones, and unstable areas.

1.2 EPA Regulatory Requirements

On April 17, 2015 the United States Environmental Protection Agency issued 40 CFR Part 257 Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule (the Rule). Sections 257.60 through 257.64 define location restriction criteria for existing CCR surface impoundments and require the owner or operator of the CCR unit to demonstrate that the unit meets minimum requirements for:

- Placement above the uppermost aquifer (§ 257.60);
- Location outside wetlands (§ 257.61);
- Location more than 60 meters (200 feet) from the outermost damage zone of a fault that has had displacement in Holocene time (§ 257.62);
- Location outside seismic impact zones (§ 257.63);
- Location away from unstable areas (§ 257.64).

Existing CCR surface impoundments, such as the Fly Ash Pond, are required to demonstrate compliance with the location restrictions by October 17, 2018. An owner or operator unable to demonstrate compliance is prohibited from placing CCR in the CCR unit under either 40 CFR § 257.60(c)(4), § 257.61(c)(4), § 257.62(c)(4), § 257.63(c)(4), or § 257.64(c)(4), as applicable unless the owner or operator complies with the alternative closure procedures specified in 40 CFR § 257.103.

1.3 Report Organization

This Demonstration Report is organized into the following sections:

<table>
<thead>
<tr>
<th>Report Section</th>
<th>Applicable CFR 40 Part 257 Citation</th>
</tr>
</thead>
<tbody>
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<td>Section 1 – Introduction</td>
<td>§ 257.60 Placement above the uppermost aquifer</td>
</tr>
<tr>
<td>Section 2 – Placement Above the Uppermost Aquifer</td>
<td>§ 257.61 Wetlands</td>
</tr>
<tr>
<td>Section 3 – Location Relative to Wetlands</td>
<td>§ 257.62 Fault areas</td>
</tr>
</tbody>
</table>

October 8, 2018
1.4 Facility Description

The Cholla Power Plant is an electric generating station located near Joseph City, in Navajo County, Arizona. The station consists of four coal-fired units. Units 1, 2 (decommissioned), and 3 are owned by APS and Unit 4 is owned by PacifiCorp. CCR generated at the Plant is either recycled for beneficial use or disposed at two major surface impoundments: the Fly Ash Pond located approximately 1.5 miles east of the Plant and the Bottom Ash Pond located about 1 mile north of the Plant. The Bottom Ash Monofill was constructed to dispose of bottom ash excavated from the Bottom Ash Pond. Lesser amounts of CCR, from the vehicle wash station, vacuum trucks, and Plant area runoff, are collected at the Sedimentation Pond. Figure 1-1 shows the location of the Fly Ash Pond in relation to the Plant.

The Fly Ash Pond is the reservoir impounded by the Fly Ash Dam, which was constructed between 1976 and 1978. The Fly Ash Pond has a total surface area of approximately 420 acres and a capacity of 18,000 acre-feet. The Fly Ash Dam is approximately 80 feet high with an approximately 4,583-foot long clay core zoned earth embankment, and has a FEMA rating of intermediate size and high hazard. The maximum permitted, normal operating water level is EL 5114.0 feet (NGVD29).

The Fly Ash Pond receives waste water that contains water and solids (fly ash and flue gas desulfurization sludge) from the Plant. The CCR wastes and other discharges are pumped from the Plant to the pond, where the CCR is allowed to settle.
2 Placement Above the Uppermost Aquifer

40 CFR § 257.60 requires that existing CCR surface impoundments must be constructed with a base that is located no less than 1.52 meters (5 feet) above the upper limit of the uppermost aquifer, unless the owner or operator demonstrates that there will not be an intermittent, recurring, or sustained hydraulic connection between any portion of the base of the CCR unit and the uppermost aquifer due to normal fluctuations in groundwater elevation (including the seasonal high water table).

_Uppermost aquifer_ is defined by the Rule to mean the geologic formation nearest the natural ground surface that is an aquifer, as well as lower aquifers that are hydraulically interconnected with this aquifer within the facility’s property boundary.

2.1 Methodology

This Location Restrictions Demonstration Report includes an assessment of the separation between the base of the Fly Ash Pond and the uppermost aquifer based on available data. The following information was reviewed to assess the vertical location of the Fly Ash Pond relative to the uppermost aquifer:

- Preconstruction topographic conditions shown on construction plans (included in Appendix A)
- Historical water level data from groundwater monitoring piezometers at the Cholla Power Plant (APS and AECOM 2016, APS 2017, and APS 2018a)

2.2 Discussion and Conclusion

2.2.1 Base Elevation of the CCR Unit

The Fly Ash Dam was constructed by building a cross-valley embankment at the downstream end of an unnamed tributary to the Little Colorado River flood plain approximately 200 feet north of Interstate 40 (see Figure 1-1). The preconstruction topography included on the construction plans (Appendix A) and design investigation boring logs (Ebasco 1975) indicate that the lowest original ground surface elevation beneath the Fly Ash Pond is at approximate EL 5048.0 feet (NGVD29).

2.2.2 Groundwater Elevations

The Fly Ash Dam is constructed on alluvium. Groundwater is present in the alluvium near the Fly Ash Pond and in the underlying bedrock aquifer. During original construction, APS installed a series of standpipe piezometers (F-104, F-105, F-108, F-109, and F-110; Figure 2-1) on the crest of the dam; these piezometers are monitored on a monthly basis. The maximum groundwater elevations for the open standpipe piezometers located in the Fly Ash Dam crest are included in the Annual CCR Impoundment and Landfill Inspection Report (APS and AECOM 2016, APS 2017, and APS 2018a) for data since 2014. The data associated with the piezometers are presented in Table 1.
Table 1 – Piezometer Data and Maximum Groundwater Elevations (ft)\(^1\)

<table>
<thead>
<tr>
<th>Location Relative to the Fly Ash Pond</th>
<th>Piezometer Name</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>F-104</td>
</tr>
<tr>
<td>Dam Crest</td>
<td></td>
</tr>
<tr>
<td>Reference Elevation (ft)</td>
<td>5121.91</td>
</tr>
<tr>
<td>Screened In</td>
<td>Alluvium and Embankment</td>
</tr>
<tr>
<td>Report Year</td>
<td>F-104</td>
</tr>
<tr>
<td>2015</td>
<td>5066.81</td>
</tr>
<tr>
<td>2016</td>
<td>5067.77</td>
</tr>
<tr>
<td>2017</td>
<td>5067.19</td>
</tr>
<tr>
<td>Highest Recorded Groundwater Elevation (ft)</td>
<td>5067.77</td>
</tr>
</tbody>
</table>

\(^1\) Elevations in Table 1 are presented in the NGVD29 datum.

2.2.3 Separation from the Uppermost Aquifer

The recently-measured water elevations in piezometers F-104, F-105, F-108, and F-110 are all higher than the estimated lowest elevation of the bottom of the Fly Ash Pond, EL 5048.0 feet (NGVD29). Prior to construction, water elevations in borings through the alluvium were observed to be between EL 5001 feet and EL 5011 feet (Ebasco 1975). As shown on the construction profile (Appendix A, Figure A-3), these groundwater elevations were within the lower section of the alluvial deposits, approximately 30 to 40 feet below the ground surface.

The rise of groundwater elevations above the original ground elevation and an apparent correlation between measured water elevations in the Fly Ash Pond and the alluvium piezometers indicate that there is a direct and sustained hydraulic connection between the water impounded in the Fly Ash Pond and the underlying alluvium.

**Conclusion:** The Fly Ash Pond does not meet the location restriction requirement relative to the uppermost aquifer and is subject to closure per 40 CFR § 257.101(b)(1).
3 Location Relative to Wetlands

40 CFR § 257.61 requires that existing surface impoundments not be located in wetlands. Wetlands are defined in 40 CFR § 232.2 as "those areas that are inundated or saturated by surface or groundwater at a frequency and duration sufficient to support, and that under normal circumstances do support, a prevalence of vegetation typically adapted for life in saturated soil conditions. Wetlands generally include swamps, marshes, bogs, and similar areas."

3.1 Methodology

The U.S. Fish and Wildlife Service (USFWS) maintains the National Wetlands Inventory mapper on the Internet (https://www.fws.gov/wetlands/data/Mapper.html). The application integrates digital map data along with other resources information to produce information on the status, extent, characteristics, and functions of wetlands and other resources. The National Wetlands Inventory, last modified on May 1, 2018, was reviewed to assess the location of the Fly Ash Pond relative to wetlands. The results are presented in Appendix C.

3.2 Discussion and Conclusion

The USFWS Wetlands Mapper indicates 10 freshwater pond and one riverine habitat in the vicinity of the Fly Ash Pond. The Mapper indicates that these ponds were photo interpreted using 1:58,000 scale, color infrared imagery from 1984. Three of the freshwater pond habitats are mapped within the impounded region of the Fly Ash Pond; however, the Fly Ash Pond had already been constructed by the time the aerial images were taken and if the bodies of water existed in the original aerial images, they would likely be the result of impounded water perched in a locally higher elevation as the reservoir level fell. The remaining seven freshwater pond habitats are between 2,000 feet and 5,000 feet away from the Fly Ash Pond and do not appear to be correlated to active seeps, perennially wet areas, or intermittently wet areas. The one riverine habitat corresponds to the Little Colorado River south of the Fly Ash Pond. Based on the age of the data in the Wetlands Mapper and the reported method of mapping, AECOM does not believe the three locations shown in the Fly Ash Pond reservoir existed as wetlands at any time.

Conclusion: The Fly Ash Pond is not located in wetlands.
4 Location Relative to Faults

40 CFR § 257.62 requires that existing surface impoundments not be located within 60 meters (200 feet) of the outermost damage zone of a fault that has had displacement in Holocene time (beginning 11,700 years before present (BP)) unless the owner or operator demonstrates the an alternative setback distance of less than 60 meters (200 feet) will prevent damage to the structural integrity of the CCR unit.

4.1 Methodology

AECOM reviewed the Quaternary Faults and Folds database maintained by the United States Geological Survey (USGS) as part of the Holocene fault search (USGS 2018). The Holocene epoch is the most recent subdivision of the Quaternary period and therefore any faults that have had displacement in the Holocene would also be included in the Quaternary period database. The Quaternary Faults and Folds database is the source for the faults used in the National Seismic Hazard Maps and contains information on faults and associated folds that are believed to be sources of M > 6 earthquakes during the Quaternary Period. AECOM searched the USGS Quaternary Fault and Fold Database for Category A and Category B faults in Navajo County, Arizona. Fault categories are defined in Table 2. Fault categories A and B relate to the Rule; fault categories C and D describe less defined or non-tectonic features.

<table>
<thead>
<tr>
<th>Category</th>
<th>Definition</th>
</tr>
</thead>
<tbody>
<tr>
<td>A</td>
<td>Geologic evidence demonstrates the existence of a Quaternary fault of tectonic origin, whether the fault is exposed by mapping or inferred from liquefaction or other deformational features.</td>
</tr>
<tr>
<td>B</td>
<td>Geologic evidence demonstrates the existence of Quaternary deformation, but either (1) the fault might not extend deeply enough to be a potential source of significant earthquakes, or (2) the currently available geologic evidence is too strong to confidently assign the feature to Class C but not strong enough to assign it to Class A.</td>
</tr>
<tr>
<td>C</td>
<td>Geologic evidence is insufficient to demonstrate (1) the existence of tectonic faulting, or (2) Quaternary slip or deformation associated with the feature.</td>
</tr>
<tr>
<td>D</td>
<td>Geologic evidence demonstrates that the feature is not a tectonic fault or feature; this category includes features such as joints, landslides, erosional or fluvial scarps, or other landforms resembling scarps but of demonstrable non-tectonic origin.</td>
</tr>
</tbody>
</table>

The Arizona Earthquake Information Center (AEIC) at Northern Arizona University maintains a catalog of earthquakes in Arizona between 1830 and 2011 (AEIC 2018). The catalog was accessed via a .kmz file to review recorded earthquakes of lower magnitude than those included in the USGS database.

4.2 Discussion and Conclusion

The USGS Quaternary Faults and Folds Database of the United States did not contain any Class A or Class B faults in Navajo County. The AEIC catalog contained one earthquake within 10 miles of the Fly Ash Pond: a Modified Mercalli intensity VI earthquake occurred near Holbrook in 1921. The earthquake location is presented in Appendix D.

Conclusion: No faults with Holocene displacement are present within 200 feet of the Fly Ash Pond.
5 Location Relative to Seismic Impact Zones

40 CFR § 257.63 requires existing surface impoundments not be located in seismic impact zones unless the owner or operator demonstrates that all structural components, including liners, leachate collection and removal systems, and surface water control systems, are designed to resist the maximum horizontal acceleration in lithified earth material for the site. *Seismic impact zone* is defined by the Rule as an area having a 2 percent or greater probability that the maximum expected horizontal acceleration, expressed as a percentage of the earth’s gravitational pull (g), will exceed 0.10 g in 50 years.

5.1 Methodology

The USGS maintains the Unified Hazard Tool website to provide access to the source and attenuation models for locations within the United States. AECOM utilized version 4.0.x of the 2014 Unified Hazard Tool to calculate the peak horizontal ground acceleration (PGA) with a 2 percent probability of exceedance in 50 years (USGS 2018a) for the Fly Ash Pond location. The Unified Hazard Tool result is presented in Appendix E.

5.2 Discussion and Conclusion

The PGA with a 2 percent probability of exceedance in 50 years for the Fly Ash Pond is 0.0878g. This value is less than the Rule-required maximum value of 0.10 g in 50 years.

*Conclusion:* The Fly Ash Pond is not located in a seismic impact zone.
6 Location Relative to Unstable Areas

40 CFR § 257.64 requires that existing surface impoundments must not be located in an unstable area unless the owner or operator demonstrates that recognized and generally accepted good engineering practices have been incorporated into the design of the CCR unit to ensure that the integrity of the structural components of the CCR unit will not be disrupted. The following factors must be considered when determining whether an area is unstable:

1) On-site or local soil conditions that may result in significant differential settling;
2) On-site or local geologic or geomorphologic features; and
3) On-site or local human-made features or events (both surface and subsurface).

**Structural components** include any component used in the construction and operation of the CCR landfill or CCR surface impoundment that is necessary to ensure the integrity of the unit and to ensure that the contents will not be released to the environment, including liners, leachate collection system, embankments, spillways, outlets, final covers, inflow design flood control systems.

**Unstable area** means a location that is susceptible to natural or human-induced events or forces capable of impairing the integrity, including structural components of some or all of the CCR unit that are responsible for preventing releases from such unit. Unstable areas can include poor foundation conditions, areas susceptible to mass movements, and karst terrains.

6.1 Methodology

The location of the Fly Ash Pond relative to unstable areas was assessed by reviewing design and construction documentation, historical geologic and geotechnical investigations, and engineering analyses (safety factor calculations). Information was reviewed to assess: 1) whether poor foundation conditions may exist which could result in inadequate foundation support for structural components of the Fly Ash Pond; or 2) whether areas susceptible to mass movement (such as landslides, avalanches, debris slides and flows, block sliding or rock falls) capable of impairing the integrity of the structural components of the Fly Ash Pond are present.

Published geologic references documenting the Holbrook Basin salt karst subsidence features and Interferometric Synthetic Aperture Radar (InSAR) data collected by the Arizona Department of Water Resources (ADWR) Satellite Based Land Subsidence Monitoring Program to monitor the spatial extent, deformation rates, and time-series history of land subsidence features identified in the state were reviewed to assess the potential for karstic terrain in the vicinity of the Fly Ash Pond.

6.2 Discussion and Conclusion

6.2.1 Geologic Setting

The Cholla Power Plant is located within the Navajo section of the Colorado Plateau Physiographic Province. The Colorado Plateau is characterized by wide areas of nearly flat-lying sedimentary rocks, separated by abrupt monoclinal folds formed when sedimentary rocks overly deep basement faults. The northwest-southeast trending Holbrook anticline occurs approximately 20 miles south of the Plant. The Navajo section is a somewhat poorly defined structural depression consisting of broad plateaus and wide valleys (Hendricks 1985). The plant is located approximately ½ mile north of the Little Colorado River. Exposed bedrock units in the vicinity of the Plant include the Permian-age Coconino Sandstone, the Triassic-age Moenkopi and Chinle Formations, and the Quaternary alluvial deposits of the Little Colorado River. Surficial geology at the Plant site consists of up to 200 feet of heterogeneous interbedded sand, silt, and clay layers of the Little Colorado River alluvium (Montgomery & Associates 2011).
The impoundment is surrounded on its north and east sides by natural topography consisting of rock outcrops of mudstones, siltstones, and sandstones.

6.2.2 Foundation Conditions

The Fly Ash Dam embankment is founded on alluvium overburden associated with an unnamed tributary to the Little Colorado River. The abutments are founded on rock consisting of mudstone, siltstone, and sandstone associated with the Moenkopi Formation.

The as-built drawings of the dam and construction inspection reports prepared by ADWR (formerly the Arizona Water Commission) indicate a cutoff trench was excavated at the abutments to extend the clay core to bedrock when the depth to bedrock was less than 20 feet. When the depth to bedrock was greater than 20 feet, a soil-bentonite slurry cutoff wall was installed to the bedrock. The construction records indicate that where the cutoff trench was excavated to bedrock, loose rock was scaled from the foundation, dental concrete was applied to irregularities to create a relatively level surface, and a thin lift of wet cement tack coat was applied to the bedrock surface before placement of the clay core. For the shell of the dam, which is founded on alluvium overburden soils, the alluvium foundation was proof-compacted using a heavy dynamic compactor and surface stringers of sandy soils that crossed the dam foundation were removed.

Several seepage locations have been observed downstream of the dam since the Fly Ash Pond went into operation. These seeps are thought to occur due to a combination of normal flow through the embankment, discontinuities in the foundation near the groin of the abutment, and flow through gypsum seams in the Moenkopi Formation. An underground French drain system was installed at the toe of the Fly Ash Dam at the Geronimo Seep and further downstream at the Hunt Seep. The seepage intercept systems pump the water collected in the sumps back into the Fly Ash Pond. A third seep along Interstate 40 (I-40), known as the I-40 Seep, is an area of seepage observed along the shoulder of I-40 where the rock outcrop near the northwest abutment was cut as part of the road construction. The I-40 Seep does not normally result in ponded water along the road and is not connected to the seepage pumpback system. The locations of these three seeps are shown in Figure 1-2. APS monitors flows from the sumps installed at the Geronimo and Hunt Seeps on a regular basis. Flow rates at the Geronimo Seep typically range from 10 to 45 gallons per minute (gpm) and flow rates at the Hunt Seep typically range from 0 to 15 gpm. The turbidity of the seep water observed at the sumps is also low. Both the low flow rate and the lack of turbidity indicate a low potential of internal erosion of the dam embankment or foundation.

6.2.3 Areas Susceptible to Mass Movement

Design and construction documentation indicate that the Fly Ash Dam was not constructed on materials that would be susceptible to excessive settlement. Furthermore, any post-construction settlement would have occurred during the nearly 40 years since construction was completed. Safety factors calculated for the Fly Ash Dam indicate that the embankment is not susceptible to mass movement (AECOM 2016). Topographic and geologic conditions do not indicate the potential for landslides, avalanches, debris slides and flows, block sliding, rock falls, or other mass movements which could impact the structural components of the Fly Ash Pond.

6.2.4 Karst Areas

Collapse features (sinkholes, fissures, depressions, expanded bedrock joints and joint sets, compression ridges and buckles) associated with dissolution of evaporate deposits within the Permian-aged Supai Formation have been documented within the Holbrook Basin (see map in Appendix F). These features, collectively referred to as "salt karst," are concentrated along a roughly 60 mile long, northwest-southeast trending dissolution front near the southwestern margin of the Holbrook Basin, approximately 20 miles from the Cholla Power Plant.

The Cholla Power Plant site is within the Holbrook Basin where ADWR monitors several land subsidence features. ADWR monitors the extent and rate of land subsidence annually using InSAR data. Land subsidence maps published by ADWR for the Holbrook Basin are included in Appendix F. Three features in the Holbrook Basin are located approximately 11 miles from the Plant site and are associated with evaporite karst dissolution. A fourth land subsidence feature has been identified south of Joseph City, approximately 2 miles southwest of the Plant site. No land subsidence features have been identified at the Plant site.
6.2.5 Subsidence

Extraction of a groundwater resource can cause lowering of the regional groundwater table, consolidation of alluvial deposits, and lowering of the ground surface. In extreme circumstances, in combination with variations in the bedrock surface, earth fissures can form and express at the ground surface around the boundary of the subsidence area. The ADWR land subsidence maps (Appendix F) indicate the presence of a 1-mile wide localized subsidence area approximately 2 miles west of the Plant, 3 miles southwest of the Bottom Ash Pond and Bottom Ash Monofill, and 3.5 miles west of the Fly Ash Pond.

The InSAR data suggest subsidence rates in the range of 0 to 1 centimeters per year (cm/yr) for the most recent six-year interval (2012-2018). APS operates a wellfield south and east of the Plant, east of the subsidence area indicated on the ADWR land subsidence maps (Appendix F). APS staff report that: 1) APS groundwater extraction from its wellfield has decreased by approximately one-third since the retirement of Unit 2 in 2014 and 2) the Coconino aquifer is highly productive and groundwater levels within the wellfield have been rising since the retirement of Unit 2 in 2014 (APS Internal Communication 2018b).

The ADWR land subsidence maps suggest a cumulative subsidence of 3.9 to 5.9 inches between 2012 and 2018. The ground underlying the Fly Ash Pond is not considered to be susceptible to the formation of earth fissures based on the distance of the CCR unit from the area of identified subsidence and the relatively small indicated total settlement.

**Conclusion:** The Fly Ash Pond is not located in an unstable area.
7 Conclusions

Based on the findings and results of the location restrictions demonstrations, AECOM provides the following conclusions for the Fly Ash Pond.

- The Fly Ash Pond does not meet the location restriction requirement relative to the uppermost aquifer and is subject to closure per 40 CFR § 257.101(b)(1).
- The Fly Ash Pond is not located in wetlands.
- No faults with Holocene displacement are present within 200 feet of the Fly Ash Pond.
- The Fly Ash Pond is not located in a seismic impact zone.
- The Fly Ash Pond is not located in an unstable area.
8 Limitations

This report is for the sole use of APS on this project only and is not to be used for other projects. In the event that conclusions based upon the data obtained in this report are made by others, such conclusions are the responsibility of others. The Certification of Professional Opinion is limited to the information available to AECOM at the time this report was written. This report was written in accordance with current practice and the standard of care. Standard of care is defined as the ordinary diligence exercised by fellow practitioners in this area performing the same services under similar circumstances during the same period. Professional judgments presented herein are primarily based on information from previous reports that were assumed to be accurate partly based on knowledge of the site and partly based on our general experience with similar evaluations performed for similar structures. No warranty or guarantee, either express or implied, is applicable to this work.

The use of the words “certification” and/or “certify” in this document shall be interpreted and construed as a Statement of Professional Opinion and is not and shall not be interpreted or construed as a guarantee, warranty, or legal opinion.
9 References


Figures
Appendix A.
Construction Plans
Appendix B.
Groundwater Elevations
Appendix C.
National Wetland Inventory
Fly Ash Pond

August 10, 2018

Wetlands
- Estuarine and Marine Deepwater
- Estuarine and Marine Wetland
- Freshwater Emergent Wetland
- Freshwater Forested/Shrub Wetland
- Freshwater Pond
- Lake
- Other
- Riverine

This map is for general reference only. The US Fish and Wildlife Service is not responsible for the accuracy or currentness of the base data shown on this map. All wetlands related data should be used in accordance with the layer metadata found on the Wetlands Mapper web site.
Appendix D.
AEIC Earthquakes
Appendix E.
Unified Hazard Tool Summary
Unified Hazard Tool

Please do not use this tool to obtain ground motion parameter values for the design code reference documents covered by the U.S. Seismic Design Maps web tools (e.g., the International Building Code and the ASCE 7 or 41 Standard). The values returned by the two applications are not identical.

<table>
<thead>
<tr>
<th>Input</th>
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<td><strong>Edition</strong></td>
<td><strong>Spectral Period</strong></td>
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<td>Conterminous U.S. 2014 (v4.0.x)</td>
<td>Peak ground acceleration</td>
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<tr>
<td><strong>Latitude</strong></td>
<td><strong>Time Horizon</strong></td>
</tr>
<tr>
<td>Decimal degrees</td>
<td>Return period in years</td>
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<td>34.933182</td>
<td>2475</td>
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<td><strong>Longitude</strong></td>
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<td>Decimal degrees, negative values for western long...</td>
<td></td>
</tr>
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<td>-110.265058</td>
<td></td>
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<td><strong>Site Class</strong></td>
<td></td>
</tr>
<tr>
<td>760 m/s (B/C boundary)</td>
<td></td>
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</tbody>
</table>
Hazard Curve

View Raw Data

https://earthquake.usgs.gov/hazards/interactive/
Appendix F.
Karst and Land Subsidence Maps
Figure 1. Location map of Holbrook Basin, study area extent, and distribution of existing evaporite karst sinks relative to the extent of the Holbrook salt body and anticline.
Total Land Subsidence in the Holbrook Basin, Navajo County
Based on Radarsat-2 Satellite Interferometric Synthetic Aperture Radar (InSAR) Data
Time Period of Analysis: 5.5 Years 09/22/2012 To 04/24/2018

Explanation
09/22/2012 To 04/24/2018
Total Land Subsidence
- Decorrelation/No Data
- Greater 40 cm (15.7 in)
- 25 - 40 cm (9.8 - 15.7 in)
- 15 - 25 cm (5.9 - 9.8 in)
- 10 - 15 cm (3.9 - 5.9 in)
- 6 - 10 cm (2.4 - 3.9 in)
- 4 - 6 cm (1.6 - 2.4 in)
- 2 - 4 cm (0.8 - 1.6 in)
- 1 - 2 cm (0.4 - 0.8 in)
- 0 - 1 cm (0 - 0.4 in)

Subsidence Feature
- Hardrock
- Cities/Towns

Highways and Interstates
- Interstate
- US
- State
- Roads
- Railway

Decorrelation (white areas) are areas where the phase of the received satellite signal changed between satellite passes, causing the data to be unusable. This occurs in areas where the land surface has been disturbed (i.e. bodies of water, snow, agriculture areas, areas of development, etc).

Coordinate System: NAD 1983 UTM Zone 12N
Projection: Transverse Mercator
Datum: North American 1983
Units: Meter
Created: 5/15/2018
Land Subsidence Rate in the Holbrook Basin, Navajo County
Based on Radarsat-2 Satellite Interferometric Synthetic Aperture Radar (InSAR) Data

Time Period of Analysis: 5.5 Years 09/22/2012 To 04/24/2018

Explanation
09/22/2012 To 04/24/2018
Land Subsidence Rate

- Decorrelation/No Data
- Greater 7 cm/yr (2.8 in/yr)
- 5 - 7 cm/yr (2.0 - 2.8 in/yr)
- 3 - 5 cm/yr (1.2 - 2.0 in/yr)
- 2 - 3 cm/yr (0.8 - 1.2 in/yr)
- 1 - 2 cm/yr (0.4 - 0.8 in/yr)
- 0.5 - 1 cm/yr (0.2 - 0.4 in/yr)
- 0 - 0.5 cm/yr (0 - 0.2 in/yr)

Decorrelation (white areas) are areas where the phase of the received satellite signal changed between satellite passes, causing the data to be unusable. This occurs in areas where the land surface has been disturbed (i.e. bodies of water, snow, agriculture areas, areas of development, etc).

Coordinate System: NAD 1983 UTM Zone 12N
Projection: Transverse Mercator
Datum: North American 1983
Units: Meter
Created: 6/12/2018